Appendix A.41:

Bideford Pl – CPT 17200

Table 1: Site Description for Bideford Pl (CC LIQ 17 – CPT 17200).

Attribute	Yes/No			Description/Date	Symbol in Figure 1
	10-m Buffer	20-m Buffer	50-m Buffer		
Near a body of surface water or other free face features?	No	No	No	The center of the site is ~440 m to the NE from the Avon River (the free-face height is ~3 m) and ~585 m to the NW from the Avon River (the free-face height is ~1.5 m).	NA
Lateral spreading observed during the CES?	No	No	No	No lateral spreading was observed by the mapping team.[1]	NA
Nearby buildings or structures?	No	Yes	Yes	Building coverage of the 20-m and 50-m buffers is 7% and 25%, respectively. The buildings are in the SE and SW quadrants of the 20-m buffer and all quadrants of the 50-m buffer.	White Fill + Brown Outline
Sloping land?	No	No	No	Flat land, residential area	NA
Step changes in the ground surface?	No	No	No	NA	NA
Retaining walls?	No	No	No	NA	NA
Vegetation?	Yes	Yes	Yes	Trees and bushes cover 27, 26, and 23% of the 10-, 20-, and 50-m buffers, respectively. They are in the NE, SE, and SW quadrants of the 10-m buffer and all quadrants of the 20-m and 50-m buffers.	White Fill + Green Outline
Manmade changes to the site between the LiDAR surveys?	Yes	Yes	Yes	Road repair in all buffers between Dec 24, 2011 and Apr 2012. Road construction (new road) in all buffers between Oct 2012 and Dec 2012. Building removal in the SE quadrant of the 20- and 50-m buffers between Aug 2013 and Feb 2014. Building addition and pavement at the same property between Feb 2014 and Aug 2014.	Building Removal/ Addition: Orange Crossline
Other important factors?	Yes	Yes	Yes	Low-motor-vehicle-volume, two-way roadway (Bideford Pl) occupies 36, 26, and 11% of the 10-, 20-, and 50-m buffers, respectively, and runs in the NE-SW direction through the NE and NW quadrants of all buffers.	Road: Gray Fill + Red Outline

Note: Buffer is the area within a circle of a specified radius with CPT investigations done at its center (172.675071°, -43.512497°).

[1] Canterbury Geotechnical Database. (2012). "Observed Ground Crack Locations", Map Layer CGD0400 - 23 July 2012, retrieved July 09, 2018 from https://canterburygeotechnicaldatabase.projectorbit.com/

Figure 1: Site plan with areas where ejecta-induced settlement is considered.

Note 1: Patch A (outlined in red) in the free field was selected for the settlement assessment as an area free of vegetation and structures. Other important factors considered for the patch selection were its proximity to a CPT, a property subjected to addition and/or demolition of a structure, front yard/backyard alterations (e.g., ploughing, rubble, scrap), and aerial distribution of sediment ejecta. In addition, the portion of the road within the 20-m and 50-m buffers was considered for settlement assessment. Roads as hard, relatively flat surfaces provide many ground-classified points. The LiDAR-based settlement analyses for the Sep-10 and Dec-11 EQs for Patch A and the Dec-11 EQ for Road were not considered due to the evident absence of ejecta.

Table 2: LiDAR flight error adjustments, global adjustments for the difference between average LiDAR point elevations and benchmark survey elevations, and vertical tectonic movement adjustments.

	Adjustments (mm)		
Earthquake Event(s)	LiDAR Flight Error	Global Offset[2]	Tectonic Vertical Movement
Sep-10	-50	-3	0
Feb-11	0	16	-70
Jun-11	0	38	-45
Dec-11	0	-65	0
CES	-50	-14	-115
Any LiDAR survey affected by ejecta?			No

Note: The negative sign indicates the subtraction from the ground surface subsidence, while the positive sign indicates the addition to the ground surface subsidence.

Table 3a: LiDAR Measurement Error for Patch A.

Surveys	Buffer	Area Averaged Difference Indicating Repeat Measurement Error (mm)	σ*$_{individual}$ LiDAR points (mm)	%Reduction in σ due to Area Averaging of LiDAR Points
Post Feb 2011: Mar 2011 and May 2011	10-m	ND	59	[17,17]
	20-m	10		
	50-m	10		
Post Dec 2011: Feb 2012 and Oct 2015	10-m	ND	70	[ND,ND]
	20-m	ND		
	50-m	ND		

*Standard deviation; ND = Not determined.

[2] Russell, J., & van Ballegooy, S. (2015). *Canterbury Earthquake Sequence: Increased liquefaction vulnerability assessment methodology*. New Zealand: Tonkin & Taylor Ltd.

Table 3b: LiDAR Measurement Error for Road.

Surveys	Buffer	Area Averaged Difference Indicating Repeat Measurement Error (mm)	б* $_{individual\ LiDAR\ points}$ (mm)	%Reduction in б due to Area Averaging of LiDAR Points
Post Feb 2011: Mar 2011 and May 2011	10-m	ND	59	[24,34]
	20-m	20		
	50-m	14		
Post Dec 2011: Feb 2012 and Oct 2015	10-m	ND	70	[ND,ND]
	20-m	ND		
	50-m	ND		

*Standard deviation; ND = Not determined.

Table 4a: Ground surface subsidence adjustments due to LiDAR measurement error for Patch A.

Earthquake Event(s)	б $_{pre\text{-}EQ\ LiDAR\ survey}$ (mm)	б $_{post\text{-}EQ\ LiDAR\ survey}$ (mm)	б $_{total}$ (mm)	Area Average Adjusted б (mm) **
Sep-10	158	56	134	±23
Feb-11	56	59	59	±10
Jun-11	59	61	62	±11
Dec-11	61	70	87	±15
CES	158	70	124	±21

**Based on the highest %Reduction in Table 3a.

Table 4b: Ground surface subsidence adjustments due to LiDAR measurement error for Road.

Earthquake Event(s)	б $_{pre\text{-}EQ\ LiDAR\ survey}$ (mm)	б $_{post\text{-}EQ\ LiDAR\ survey}$ (mm)	б $_{total}$ (mm)	Area Average Adjusted б (mm) **
Sep-10	158	56	134	±45
Feb-11	56	59	59	±20
Jun-11	59	61	62	±21
Dec-11	61	70	87	±29
CES	158	70	124	±42

**Based on the highest %Reduction in Table 3b.

Table 5a: Raw liquefaction-related ground surface subsidence using original LiDAR points for Patch A.

Earthquake Event(s)	Average Ground Surface Subsidence (mm)		
	10-m Buffer	20-m Buffer	50-m Buffer
Sep-10	ND	ND	ND
Feb-11	ND	215	215
Jun-11	ND	45	45
Dec-11	ND	ND	ND
CES	ND	ND	ND

Table 5b: Raw liquefaction-related ground surface subsidence using original LiDAR points for Road.

Earthquake Event(s)	Average Ground Surface Subsidence (mm)		
	10-m Buffer	20-m Buffer	50-m Buffer
Sep-10	ND	58	57
Feb-11	ND	155	155
Jun-11	ND	50	49
Dec-11	ND	ND	ND
CES	ND	ND	ND

Table 6a: Corrected liquefaction-related ground surface subsidence using original LiDAR points for Patch A with the calculated adjustments in Table 2.

Earthquake Event(s)	Average Calculated Ground Surface Subsidence (mm)		
	10-m Buffer	20-m Buffer	50-m Buffer
Sep-10	ND	ND	ND
Feb-11	ND	161±25	161±25
Jun-11	ND	38±25	38±25
Dec-11	ND	ND	ND
CES	ND	ND	ND

Notes: Plus/minus values are same as those in Table 4a, but rounded to the nearest 25 mm; Positive overall values indicate ground surface subsidence, while negative overall values indicate ground surface uplift; ND = Not determined.

Table 6b: Corrected liquefaction-related ground surface subsidence using original LiDAR points for Road with the calculated adjustments in Table 2.

	Average Calculated Ground Surface Subsidence (mm)		
Earthquake Event(s)	10-m Buffer	20-m Buffer	50-m Buffer
Sep-10	ND	5±50	4±50
Feb-11	ND	101±25	101±25
Jun-11	ND	43±25	42±25
Dec-11	ND	ND	ND
CES	ND	ND	ND

Notes: Plus/minus values are same as those in Table 4b, but rounded to the nearest 25 mm; Positive overall values indicate ground surface subsidence, while negative overall values indicate ground surface uplift; ND = Not determined.

Table 7a: Corrected liquefaction-related ground surface subsidence for Patch A using LiDAR DEMs.

	Estimated Ground Surface Subsidence (mm)								
	10-m Buffer			20-m Buffer			50-m Buffer		
Earthquake Event(s)	16th %ile	50th %ile	84th %ile	16th %ile	50th %ile	84th %ile	16th %ile	50th %ile	84th %ile
Sep-10	50	100	100	50	100	100	50	100	100
Feb-11	150	150	150	150	150	150	150	150	150
Jun-11	50	50	50	50	50	50	50	50	50
Dec-11	<50	<50	50	<50	<50	50	<50	<50	50
CES	300	300	300	300	300	300	300	300	300

Note: These percentiles are not the exact statistical measures; they indicate the spatial variability of ground surface subsidence.

Table 7b: Corrected liquefaction-related ground surface subsidence for Road using LiDAR DEMs.

	Estimated Ground Surface Subsidence (mm)								
	10-m Buffer			20-m Buffer			50-m Buffer		
Earthquake Event(s)	16th %ile	50th %ile	84th %ile	16th %ile	50th %ile	84th %ile	16th %ile	50th %ile	84th %ile
Sep-10	<50	<50	50	<50	<50	50	<50	<50	50
Feb-11	50	100	150	50	100	150	50	100	150
Jun-11	50	50	50	50	50	50	50	50	50
Dec-11	<50	<50	<50	<50	<50	<50	<50	<50	<50
CES	150	200	200	150	200	200	150	200	200

Note: These percentiles are not the exact statistical measures; they indicate the spatial variability of ground surface subsidence.

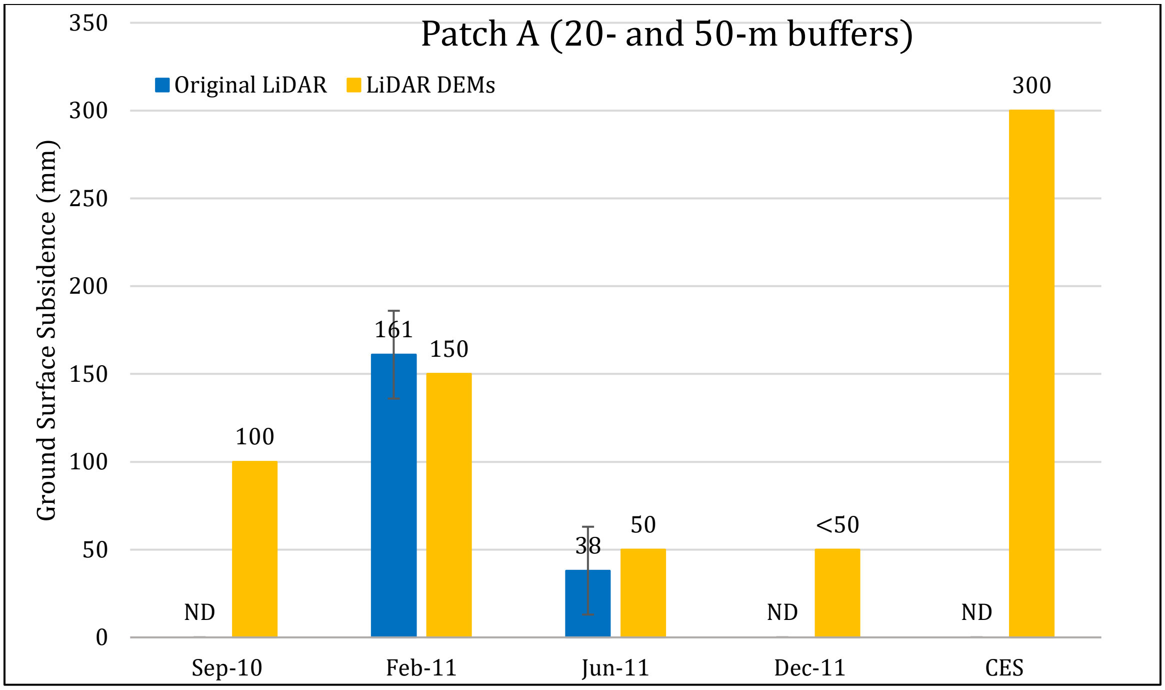

Figure 2: Comparison between ground surface subsidence determined from original LiDAR survey points and ground surface subsidence (50th %ile) estimated using LiDAR DEMs for Patch A.

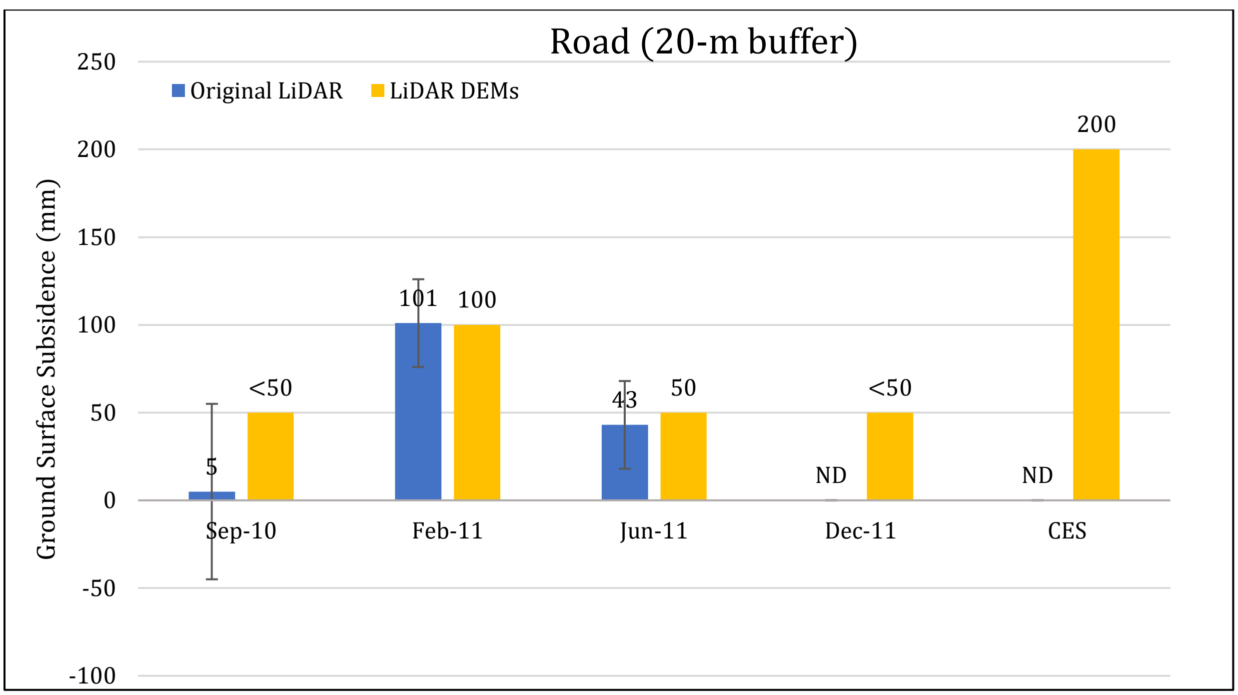

Figure 3: Comparison between ground surface subsidence determined from original LiDAR survey points and ground surface subsidence (50th %ile) estimated using LiDAR DEMs for Road (20-m buffer).

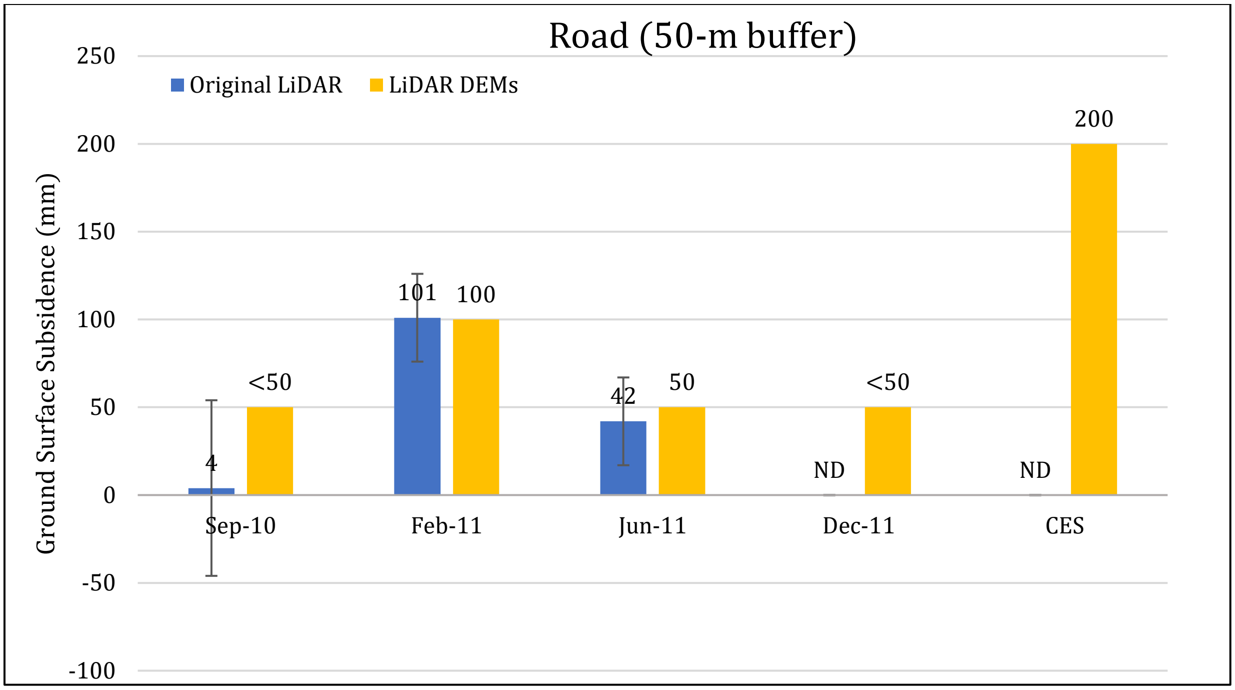

Figure 4: Comparison between ground surface subsidence determined from original LiDAR survey points and ground surface subsidence (50th %ile) estimated using LiDAR DEMs for Road (50-m buffer).

Note 2: The ground surface subsidence values determined from original LiDAR survey points are similar to the ground surface subsidence values estimated using LiDAR DEMs for all earthquake events.

Table 8a: Ejecta-Induced settlement for the top 20 m of the soil profile for Patch A for the 50th %ile PGA, P_L=50%, and C_{FC}=0.13 using BI-2014, ZRB-2002, and I_C cutoff of 2.6.

Earthquake Event(s)	M_W	PGA (g)	Depth to Groundwater (m)	S_T (mm)	S_{V1D} (mm)	$S_{E,L}$ (mm)
Sep-10	7.1	0.19	2.5	ND	4±20	ND
Feb-11	6.2	0.43	1.7	161±25	52±50	109±56
Jun-11	6.2	0.26	2.5	38±25	10±25	28±35
Dec-11	6.1	0.28	2.0	ND	26±50	ND

Notes: S_T = Total settlement (Table 6); S_{V1D} = Average vertical settlement due to volumetric compression using Boulanger and Idriss (2014) (BI-2014), Zhang et al. (2002) (ZRB-2002) procedures and de Greef and Lengkeek (2018) thin-layer correction; $S_{E,L}$ = Ejecta-induced settlement as the difference between the LiDAR-based S_T and S_{V1D}.

Table 8b: Ejecta-Induced settlement for the top 20 m of the soil profile for Road (20-m buffer) for the 50th %ile PGA, P_L=50%, and C_{FC}=0.13 using BI-2014, ZRB-2002, and I_C cutoff of 2.6.

Earthquake Event(s)	M_W	PGA (g)	Depth to Groundwater (m)	S_T (mm)	S_{V1D} (mm)	$S_{E,L}$ (mm)
Sep-10	7.1	0.19	2.5	5±50	2±20	3±54
Feb-11	6.2	0.43	1.7	101±25	38±50	63±56
Jun-11	6.2	0.26	2.5	43±25	5±25	38±35
Dec-11	6.1	0.28	2.0	ND	9±50	ND

Notes: S_T = Total settlement (Table 6); S_{V1D} = Average vertical settlement due to volumetric compression using Boulanger and Idriss (2014) (BI-2014), Zhang et al. (2002) (ZRB-2002) procedures and de Greef and Lengkeek (2018) thin-layer correction; $S_{E,L}$ = Ejecta-induced settlement as the difference between the LiDAR-based S_T and S_{V1D}.

Table 8c: Ejecta-Induced settlement for the top 20 m of the soil profile for Road (50-m buffer) for the 50th %ile PGA, P_L=50%, and C_{FC}=0.13 using BI-2014, ZRB-2002, and I_C cutoff of 2.6.

Earthquake Event(s)	M_W	PGA (g)	Depth to Groundwater (m)	S_T (mm)	S_{V1D} (mm)	$S_{E,L}$ (mm)
Sep-10	7.1	0.19	2.5	4±50	4±20	0±54
Feb-11	6.2	0.43	1.7	101±25	60±50	41±56
Jun-11	6.2	0.26	2.5	42±25	11±25	31±35
Dec-11	6.1	0.28	2.0	ND	19±50	ND

Notes: S_T = Total settlement (Table 6); S_{V1D} = Average vertical settlement due to volumetric compression using Boulanger and Idriss (2014) (BI-2014), Zhang et al. (2002) (ZRB-2002) procedures and de Greef and Lengkeek (2018) thin-layer correction; $S_{E,L}$ = Ejecta-induced settlement as the difference between the LiDAR-based S_T and S_{V1D}.

Note 3: The uncertainty for volumetric settlement was derived based on the sensitivity of volumetric settlement to PGA, C_{FC}, and P_L for each earthquake event for VsVp 57203 *Shirley Intermediate School* and CC LIQ 1 – CPT 5586 – *Vivian St* sites. Taking the 50th percentile as the baseline case, the minimum and maximum values corresponding to the difference between the 25th percentile and the 50th percentile and the 75th percentile and the 50th percentile were determined. The arithmetic mean of the range of the minimum and maximum difference was evaluated for each patch at the two sites. The maximum arithmetic mean for each earthquake event was rounded to the nearest five and used as the uncertainty value. Accordingly, the 1-D volumetric settlement uncertainties of ±20, ±50, ±25, and ±50 mm for the Sep-10, Feb-11, Jun-11, and Dec-11 earthquake events, respectively, were used for all sites in this study.

Table 9a: Coverage area and height of ejecta estimates for Patch A using photographs.

Earthquake Event	$H_{E,thick1}$ (mm)	$A_{E,thick1}$ (m^2)	$H_{E,thick2}$ (mm)	$A_{E,thick2}$ (m^2)	$H_{E,thin}$ (mm)	$A_{E,thin}$ (m^2)	A_T (m^2)
Sep-10	0	0	0	0	0	0	49.8
Feb-11	100-160	23.6	60-120	1.0	10-20	18.5	49.8
Jun-11	0	0	40-60	20.6	0	0	49.8
Dec-11	0	0	0	0	0	0	49.8

Notes: $A_{E,thick/thin}$ = Coverage area of thick/thin ejecta layers; $H_{E,thick/thin}$ = Lower-upper estimate of height of thick/thin ejecta layers; Thin and thick layers correspond to light gray and dark gray colors of ejecta observed in aerial photographs; A_T = Total assessment area of a buffer being considered.

Table 9b: Coverage area and height of ejecta estimates for Road (20-m buffer) using photographs.

EQ Event	$H_{E,prism/pyr}$ (mm)	$V_{E,prism+pyr}$ (m^3)	$H_{E,thin}$ (mm)	$A_{E,thin}$ (m^2)	A_T (m^2)
Sep-10	42-106	0.28-0.56	2-6	22.9	345
Feb-11	32-200	10.9-13.5	2-4	185	349
Jun-11	14-150	1.99-3.97	2-4	6.5	327*
Dec-11	0	0	0	0	349

Notes: $A_{E,thin}$ = Coverage area of thin ejecta layers; $H_{E,thin}$ = Lower-upper estimate of height of thin ejecta layers; $H_{E,prism/pyr}$ = Lower-upper estimate of ejecta height near the curb based on 2-4% cross slope of normal crown; $V_{E,prism+pyr}$ = Lower-upper estimate of total volume of prismatic- and pyramidal-shape ejecta; A_T= Total assessment area of a buffer being considered; * indicates reduction in A_T due to the presence of objects/shadows.

Table 9c: Coverage area and height of ejecta estimates for Road (50-m buffer) using photographs.

EQ Event	$H_{E,prism/pyr}$ (mm)	$V_{E,prism+pyr}$ (m^3)	$H_{E,thin}$ (mm)	$A_{E,thin}$ (m^2)	A_T (m^2)
Sep-10	33-115	1.84-3.68	2-6	28.0	914
Feb-11	21-200	29.9-33.8	2-4	334	923
Jun-11	14-150	3.68-7.35	2-4	24.4	859*
Dec-11	0	0	0	0	923

Notes: $H_{E,prism/pyr}$ = Lower-upper estimate of ejecta height near the curb based on 2-4% cross slope of normal crown; $V_{E,prism+pyr}$ = Lower-upper estimate of total volume of prismatic- and pyramidal-shape ejecta; $A_{E,thin}$ =Coverage area of thin ejecta layers; $H_{E,thin}$ = Lower-upper estimate of height of thin ejecta layers; A_T= Total assessment area of a buffer being considered; * indicates reduction in A_T due to the presence of objects/shadows.

Note 4: The values in Table 9 correspond to the coverage area of ejecta outlined in aerial photographs (Figures 28 and 63-65) and the lower and upper estimates of ejecta height based on geometrical approximations, ground photographs (Figures 67 and 68), and EQC LDAT property inspection reports (e.g., Figure 66). The ejecta-induced settlement using photographs and engineering judgment, $S_{E,P}$, is estimated as

$$S_{E,P} = \frac{\sum_{i=1}^{a} A_{E,thick,i} * H_{E,thick,i} + \sum_{j=1}^{b} A_{E,thin,j} * H_{E,thin,j}}{A_T} + \frac{\frac{1}{2}\sum_{n=1}^{f} W_{E,prism,n} * H_{E,prism,n} * L_{E,prism,n}}{A_T} + \frac{\frac{1}{3}\sum_{p=1}^{g} W_{E,r.pyramid,p} * H_{E,r.pyramid,p} * L_{E,r.pyramid,p}}{A_T} + \frac{\frac{1}{6}\sum_{r=1}^{h} W_{E,t.pyramid,r} * H_{E,t.pyramid,r} * L_{E,t.pyramid,r}}{A_T}$$

$$= \frac{\sum_{i=1}^{a} V_{E,thick,i} + \sum_{j=1}^{b} V_{E,thin,j} + \sum_{n=1}^{f} V_{E,prism,n} + \sum_{p=1}^{g} V_{E,r.pyramid,p}}{A_T} + \frac{\sum_{r=1}^{h} V_{E,t.pyramid,r}}{A_T}$$

where

- $A_{E,thick,i}$ and $H_{E,thick,i}$ are the area and the height of a thick ejecta layer, respectively;
- $A_{E,thin,j}$ and $H_{E,thin,j}$ are the area and the height of a thin ejecta layer, respectively;
- $W_{E,prism,n}$ and $L_{E,prism,n}$ are the width and the length of the coverage area of a prismatically shaped ejecta layer, respectively, and $H_{E,prism,n}$ is the height of a prism-like ejecta layer;
- $W_{E,r.pyr,p}$ and $L_{E,r.pyr,p}$ are the width and the length, respectively, of the coverage area of an ejecta layer with the rectangular base, and $H_{E,r.pyr,p}$ is the height of the rectangular-base pyramid-like ejecta layer;
- $W_{E,t.pyr,r}$ and $L_{E,t.pyr,r}$ are the width and the length, respectively, of the coverage area of an ejecta layer with the triangular base, and $H_{E,t.pyr,r}$ is the height of the triangular-base pyramid-like ejecta layer;
- A_T is the total assessment area for a buffer being considered (Figure 1).

Table 10: Ejecta-induced settlement estimates for Patch A and Road based on photographs.

Earthquake Event	Patch A		Road (20-m buffer)		Road (50-m buffer)	
	$S_{E,P,lower}$ (mm)	$S_{E,P,upper}$ (mm)	$S_{E,P,lower}$ (mm)	$S_{E,P,upper}$ (mm)	$S_{E,P,lower}$ (mm)	$S_{E,P,upper}$ (mm)
Sep-10	0	0	1	2	2	4
Feb-11	52	86	32	41	33	38
Jun-11	17	25	6	12	4	9
Dec-11	0	0	0	0	0	0

Note: $S_{E,P,lower}$ and $S_{E,P,upper}$ correspond to lower and upper estimates of $S_{E,P}$, respectively.

Table 11: Best final estimates of ejecta-induced settlement for Patch A and Road.

EQ Event	Patch A			Road (20-m buffer)			Road (50-m buffer)		
	$S_{E,L}$ (mm)	$S_{E,P}$ (mm)	$S_{E,final}$ (mm)	$S_{E,L}$ (mm)	$S_{E,P}$ (mm)	$S_{E,final}$ (mm)	$S_{E,L}$ (mm)	$S_{E,P}$ (mm)	$S_{E,final}$ (mm)
Sep-10	ND	0	0	3±54	1.5±0.5	<5	0±54	3±1	5±5
Feb-11	109±56	69±17	90±30	63±56	36.5±4.5	50±30	41±56	35.5±2.5	40±30
Jun-11	28±35	21±4	25±20	38±35	9±3	25±20	31±35	6.5±2.5	20±20
Dec-11	ND	0	0	ND	0	0	ND	0	0

Notes: $S_{E,L}$ = Ejecta-induced settlement based on LiDAR data reported in Table 8; $S_{E,P}$ = Median ejecta-induced settlement for the range of values reported in Table 10; $S_{E,final}$ = Best final estimate of ejecta-induced settlement rounded to the nearest 5 mm; Final plus/minus values are also rounded to the nearest 5 mm; ND = Not determined.

Note 5:

- Patch A: $S_{E,final}$ for the Sep-10 and Dec-11 EQs is based solely on $S_{E,P}$ due to the evident absence of ejecta. $S_{E,final}$ for the Feb-11 and Jun-11 EQ is the weighted average of $S_{E,L}$ and $S_{E,P}$ with weights of 1/2 and 1/2, respectively. The uncertainty associated with $S_{E,final}$ is also the weighted average of uncertainties associated with $S_{E,L}$ and $S_{E,P}$ with the same weights of 1/2 and 1/2, respectively.
- Road: $S_{E,final}$ for the Dec-11 EQ is based solely on $S_{E,P}$ due to the evident absence of ejecta. $S_{E,final}$ for Sep-10, Feb-11 and Jun-11 EQs is a weighted average of $S_{E,L}$ and $S_{E,P}$ with weight coefficients of 1/2 and 1/2, respectively. Likewise, the uncertainty associated with $S_{E,final}$ is a weighted average of uncertainties associated with $S_{E,L}$ and $S_{E,P}$ with the same weights of 1/2 and 1/2, respectively.
- The weight coefficients are based on the LiDAR error bands, LPI prediction error (Maurer et al. 2014[3]), presence of ejecta at the time of LiDAR surveys, density of July 2003 LiDAR points, and completeness of visual evidence (i.e., ground and aerial photographs and EQC LDAT property inspection reports for the site). The Bideford Pl site is in the apparent zone of higher ground surface subsidence for the Sep-10 EQ (i.e., the Jul-03 LiDAR flight error). The site is in the zone of accurate LPI prediction of liquefaction severity for the Sep-10 and Feb-11 EQs. The LDAT inspection report and ground photographs from 16 June 2011 are available for the property with Patch A; the approximate ejecta height at the property at the time of the inspection was recorded as 100 mm. The ejecta height at other properties within the 50-m buffer was ~50-200 mm, as per the LDAT property inspection reports from 16 June 2011. The reports are also available for the Sep-10 EQ, noting minor ejecta at two properties within the 50-m buffer. There are no ground photographs of ejecta on the road.

[3] Maurer, B. W., Green, R. A., Cubrinovski, M., & Bradley, B. A. (2014). Evaluation of the Liquefaction Potential Index for Assessing Liquefaction Hazard in Christchurch, New Zealand. *Journal of Geotechnical and Geoenvironmental Engineering*, 140(7), 04014032-1-11. doi:10.1061/(asce)gt.1943-5606.0001117

<u>Summary 1</u>:

- **The best estimate of the ejecta-induced free-field ground settlement at the Bideford Pl site for the FEB 2011, JUN 2011, and DEC 2011 earthquake is 90±30 mm, 25±20 mm, and 0 mm, respectively. For the SEP 2010, the best final estimate of the ejecta-induced settlement for <5% of the site that was covered with ejecta is <5 mm.**
- **The best estimate of the ejecta-induced free-field ground settlement of the road at the Bideford Pl site for the SEP 2010, FEB 2011, JUN 2011, and DEC 2011 earthquake is <5 mm, 50±30 mm, 25±20 mm, and 0 mm, respectively.**

Figure 5: Location of the site.

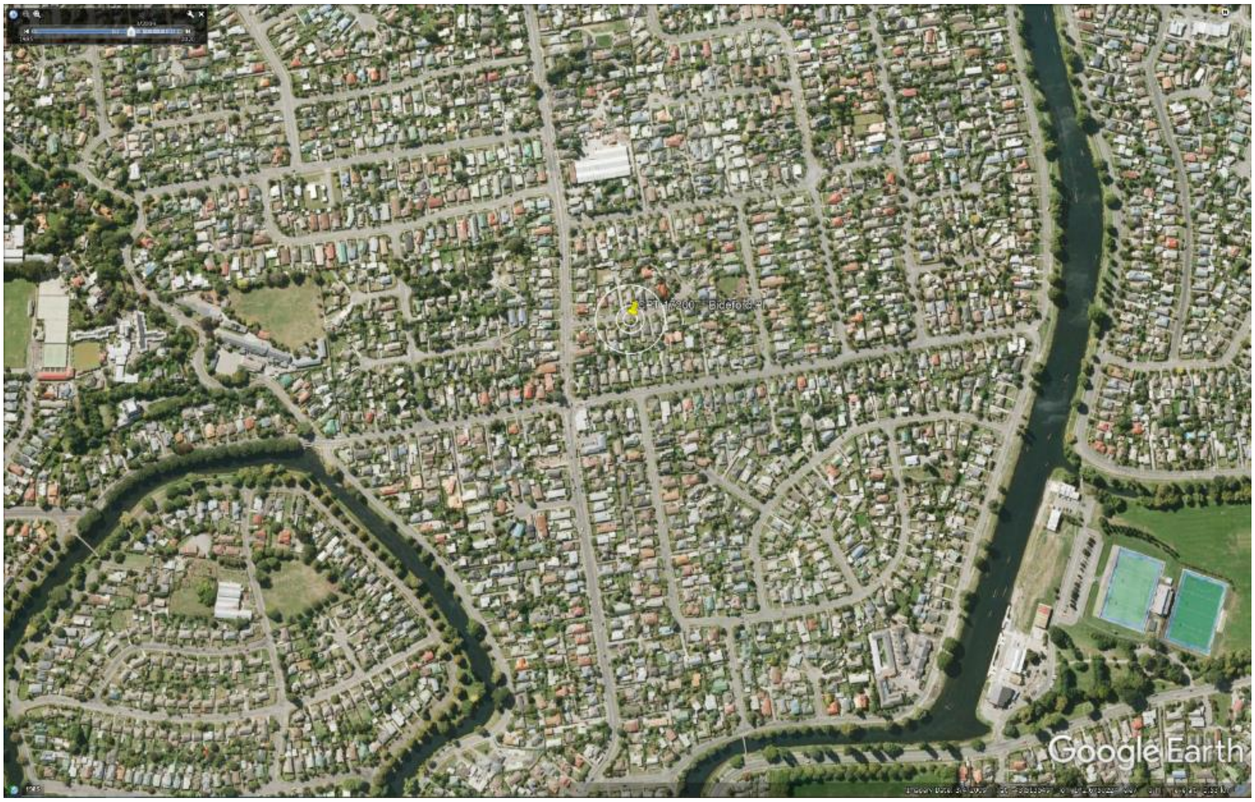

Figure 6: Position of the site relative to nearby buildings, vegetation, and free-face features.

Figure 7: Street view of the flat land.

Figure 8: Satellite image of the site taken in Dec 2004.

Figure 9: Satellite image of the site taken in Mar 2009.

Figure 10: Satellite image of the site taken on Sep 3, 2010.

Figure 11: Satellite image of the site taken on Sep 5, 2010.

Figure 12: Satellite image of the site taken on Feb 7, 2011.

Figure 13: Satellite image of the site taken on Feb 26, 2011.

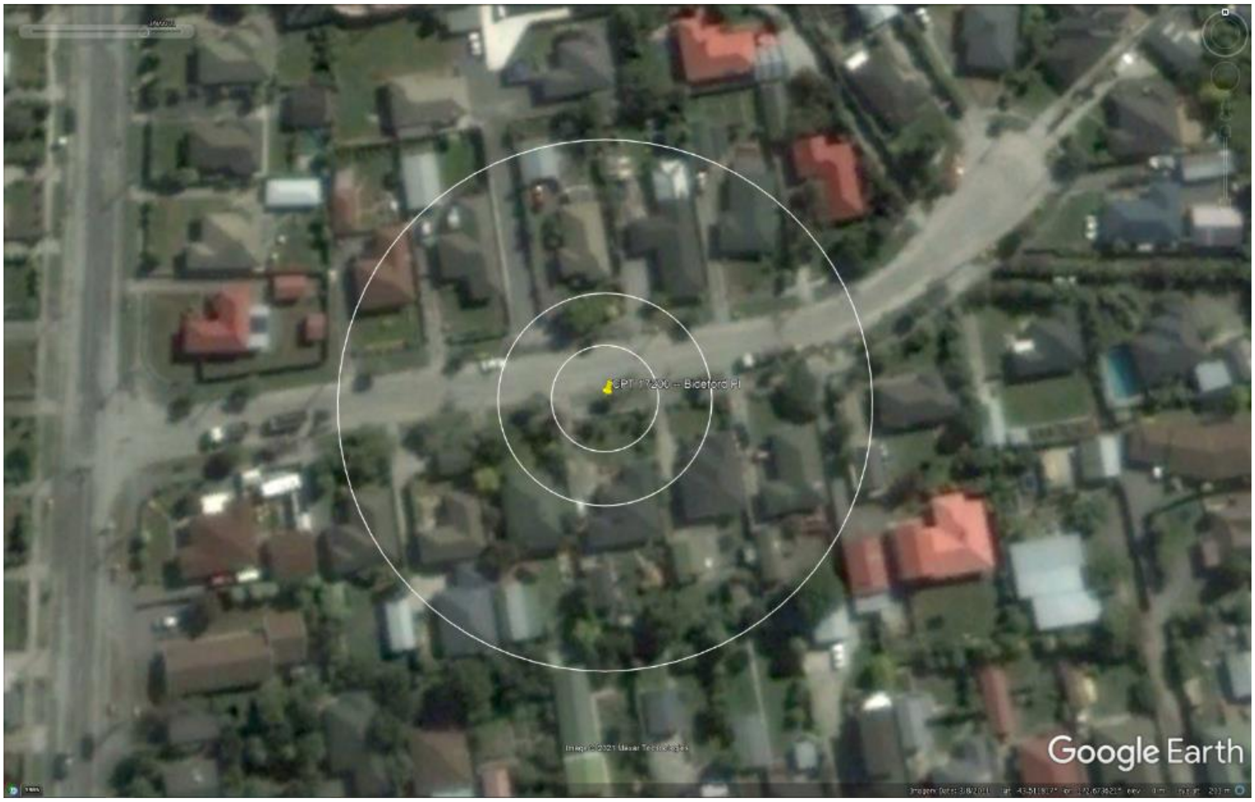

Figure 14: Satellite image of the site taken on Mar 8, 2011.

Figure 15: Satellite image of the site taken in Apr 2012.

Figure 16: Satellite image of the site taken in Oct 2012.

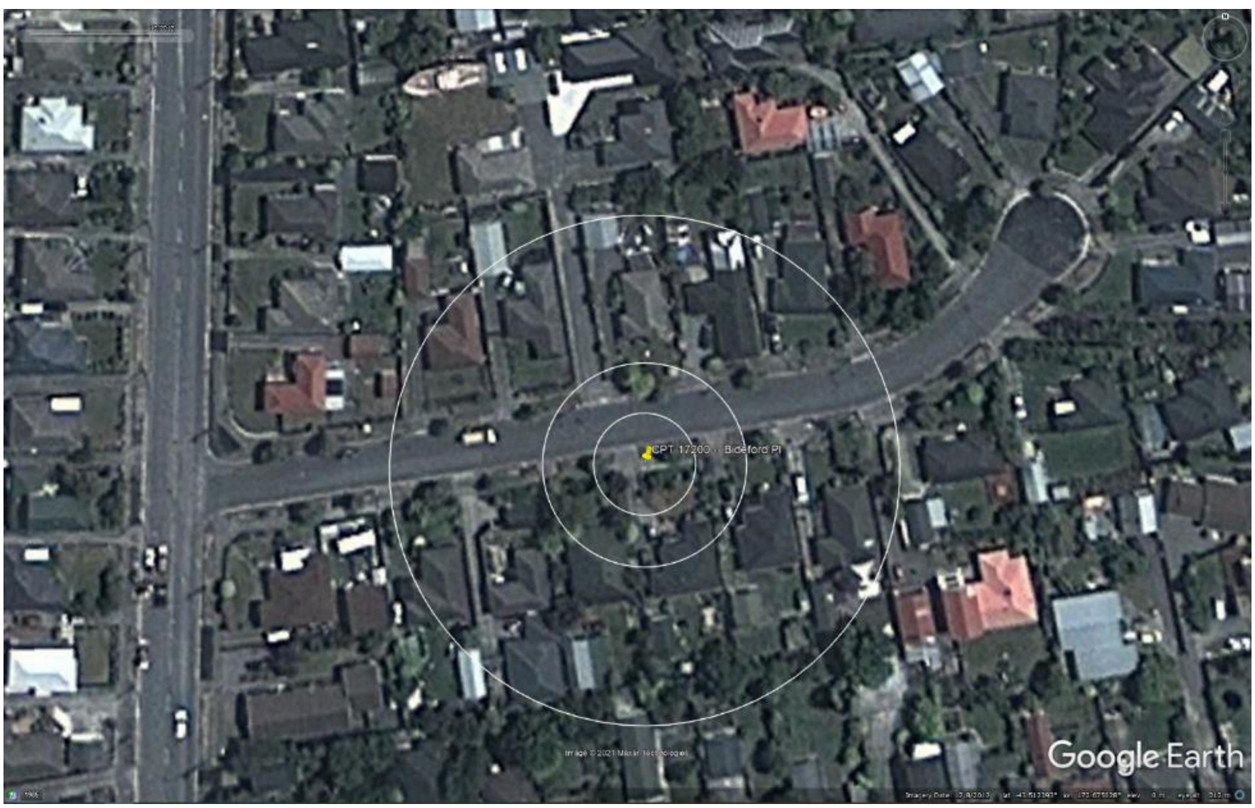

Figure 17: Satellite image of the site taken in Dec 2012.

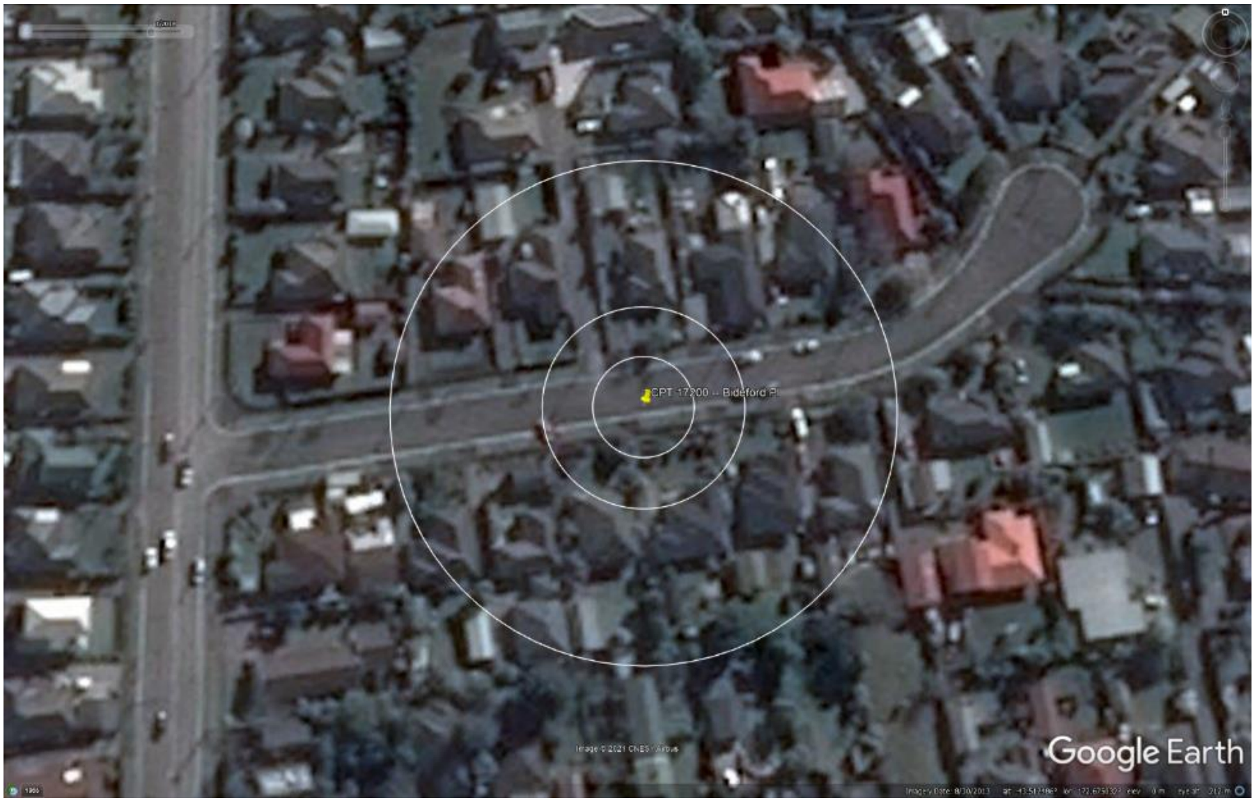

Figure 18: Satellite image of the site taken in Aug 2013.

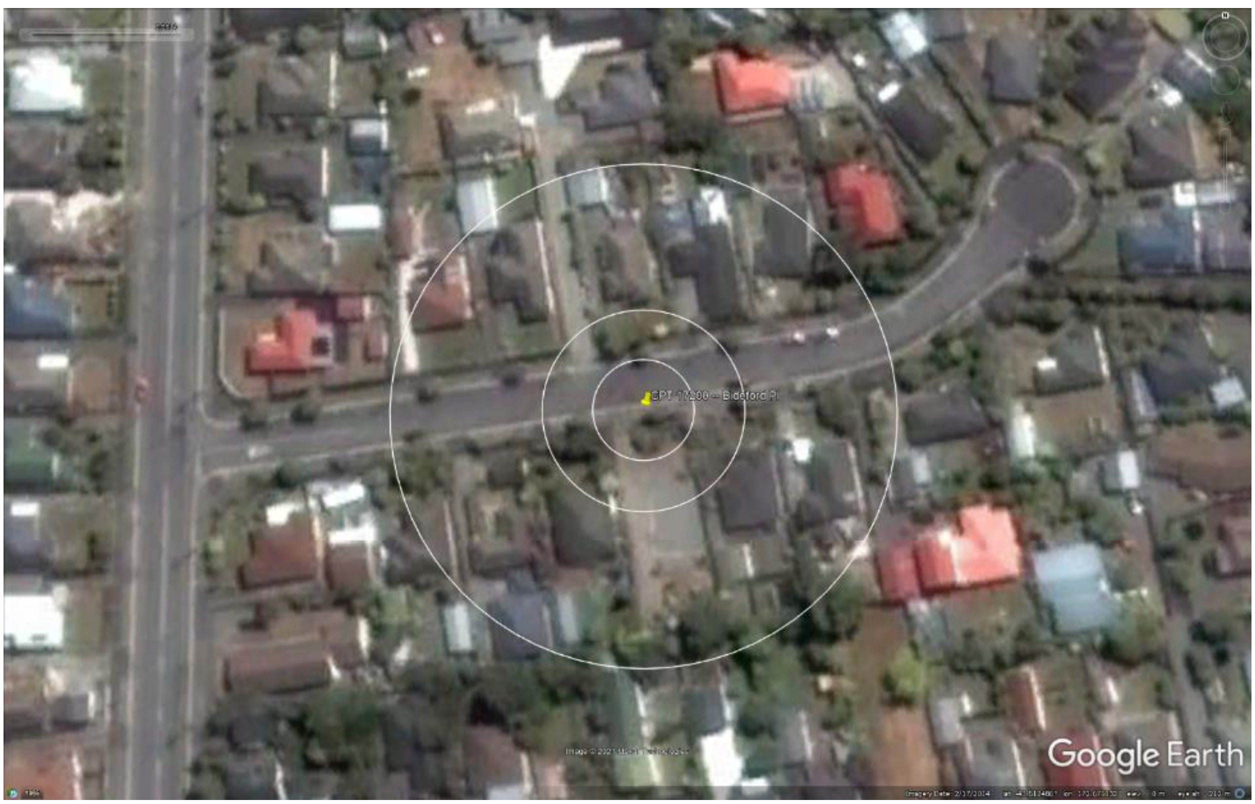

Figure 19: Satellite image of the site taken in Feb 2014.

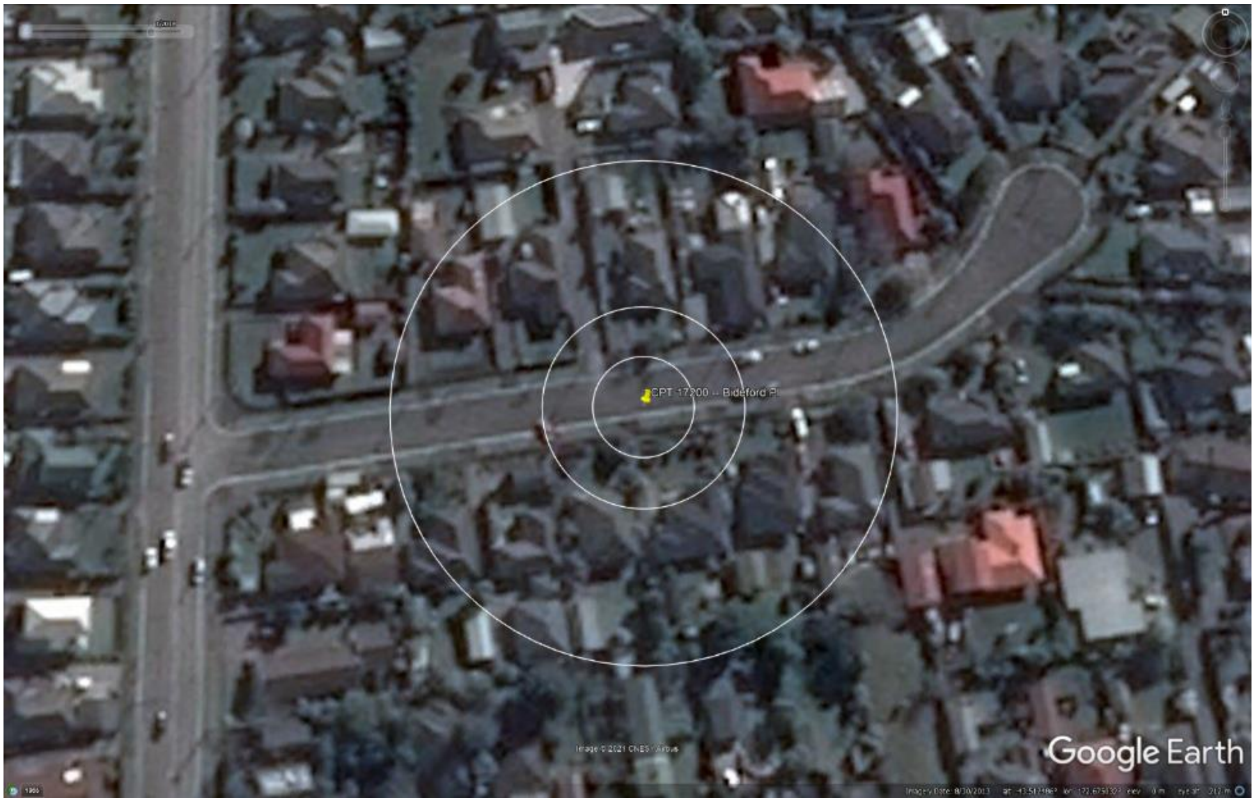

Figure 20: Satellite image of the site taken in Aug 2013.

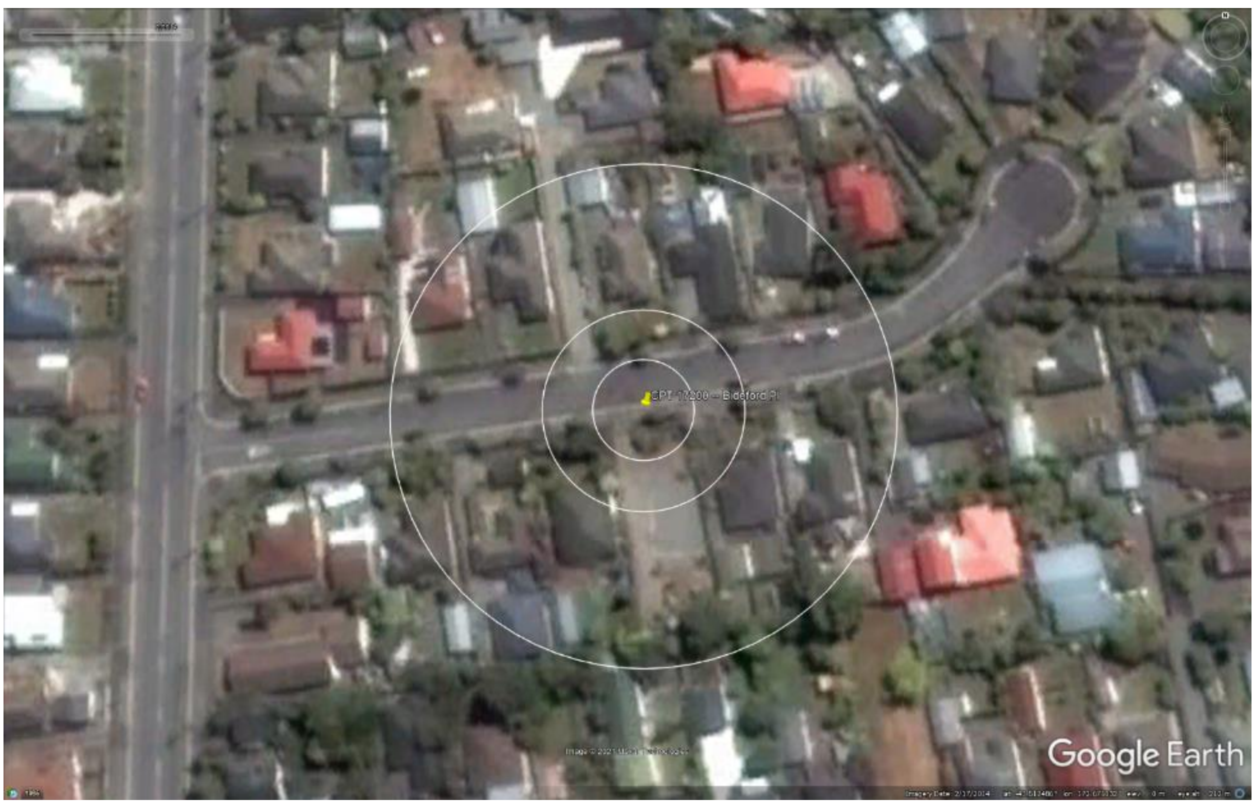

Figure 21: Satellite image of the site taken in Feb 2014.

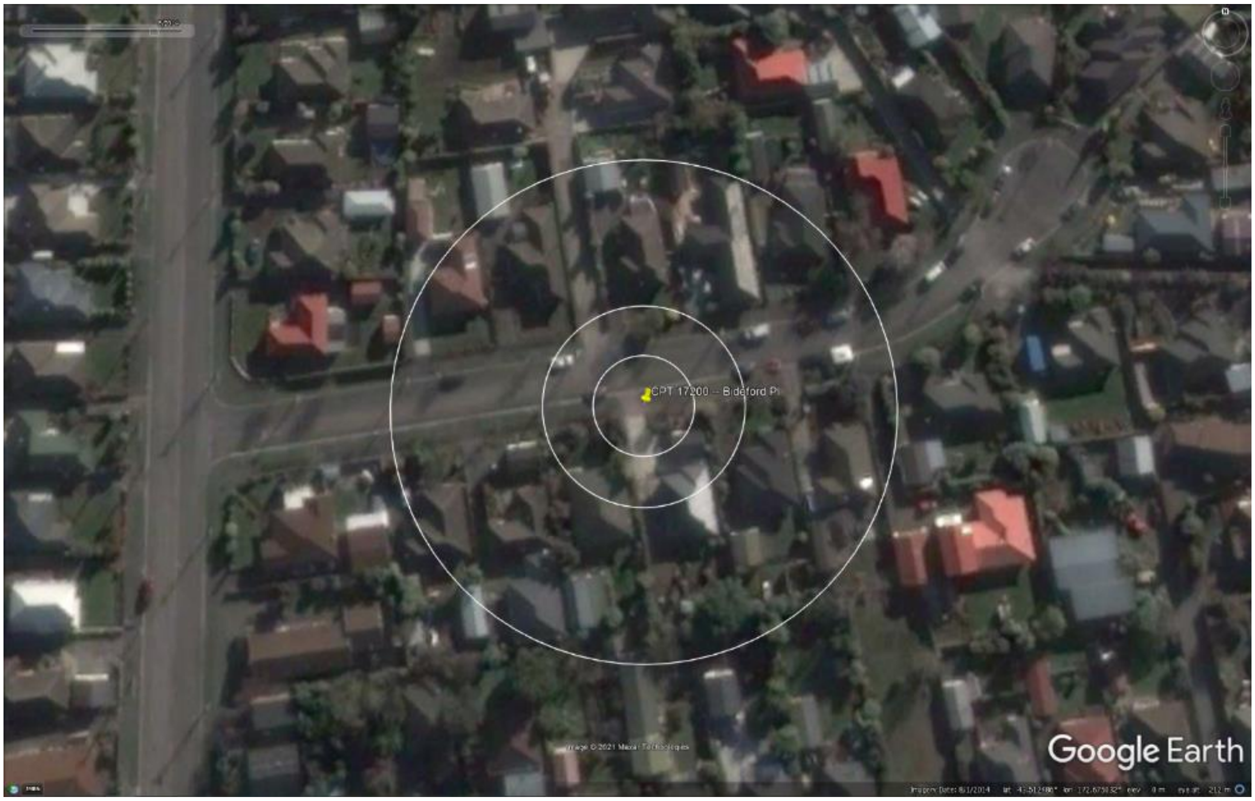

Figure 22: Satellite image of the site taken in Aug 2014.

Figure 23: Satellite image of the site taken in Nov 2015.

Figure 24: Aerial photograph of the site taken on Sep 4, 2010.

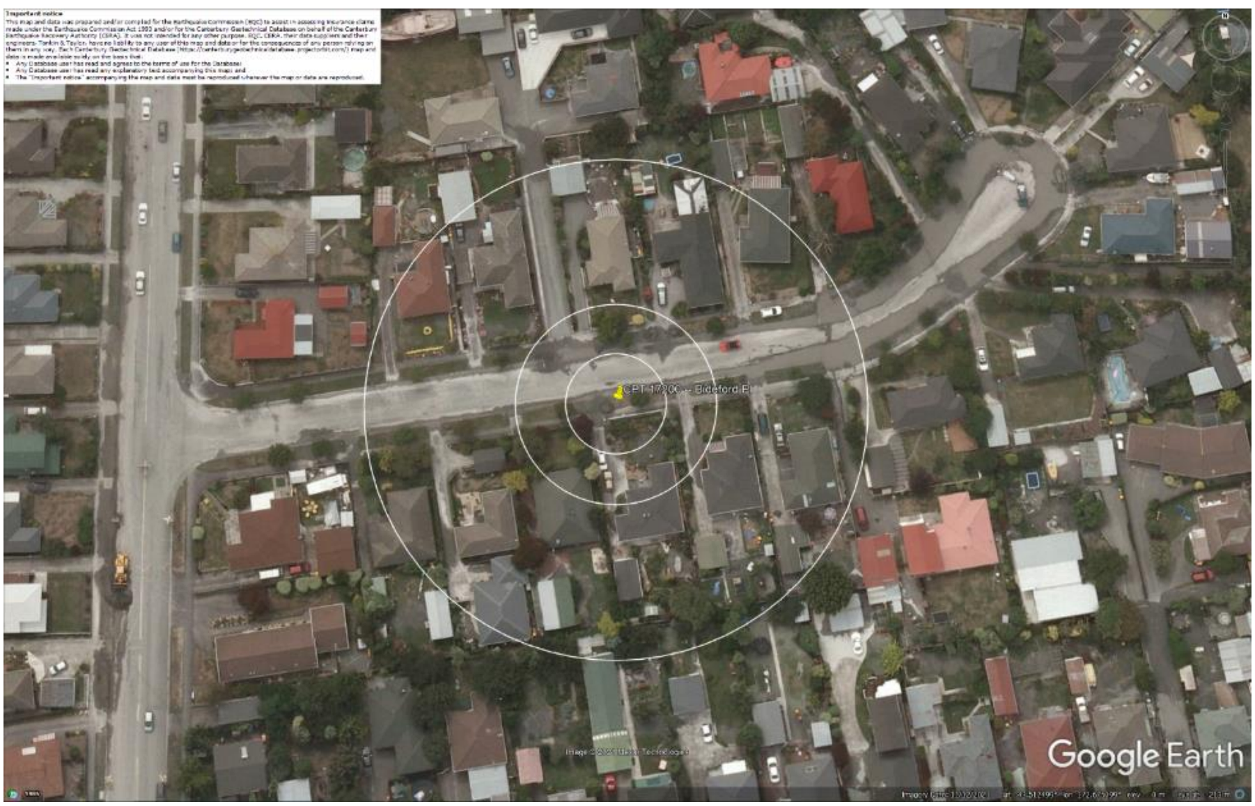

Figure 25: Aerial photograph of the site taken on Feb 24, 2011.

Figure 26: Aerial photograph of the site taken on June 14-15, 2011.

Figure 27: Aerial photograph of the site taken on June 16, 2011.

Figure 28: Aerial photograph of the site taken on Dec 24, 2011.

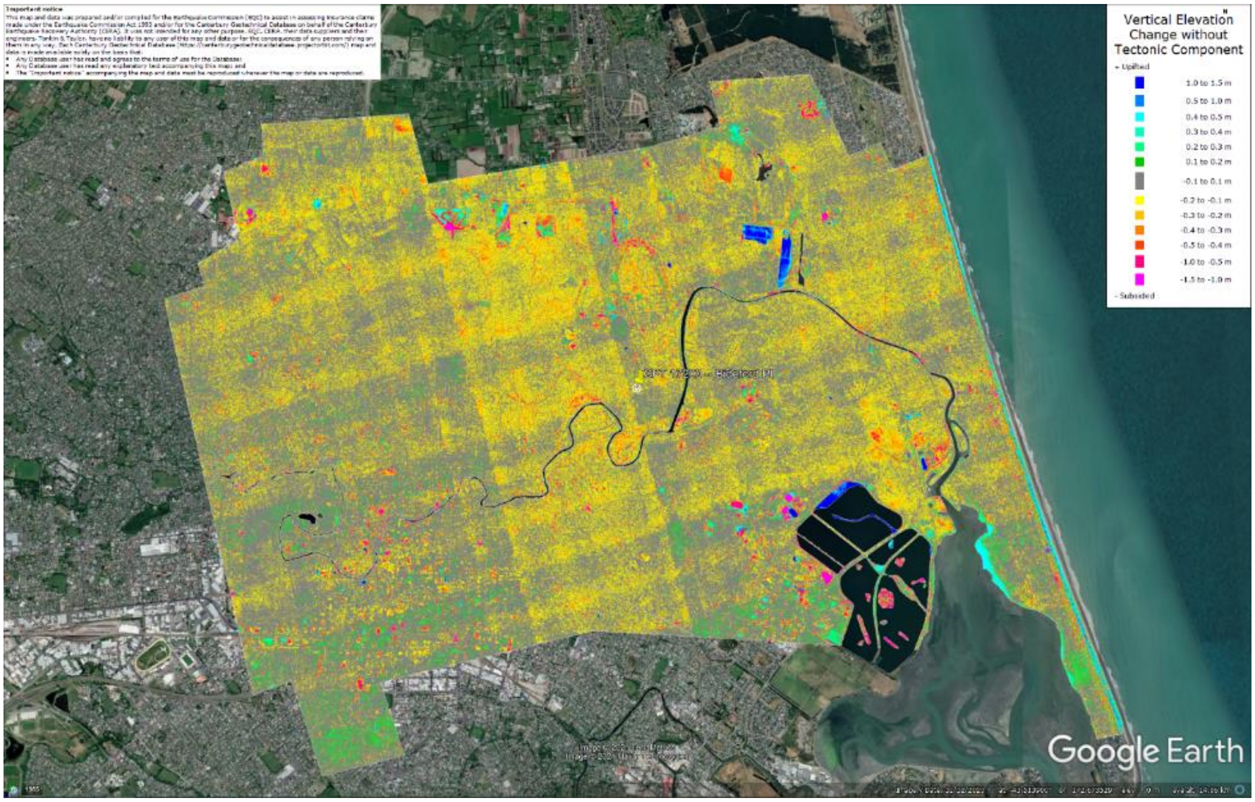

Figure 29: Vertical Ground Movements (Surface – Tectonic) for Sep 2010 Earthquake – the site is in the apparent zone of overestimated ground surface subsidence (i.e., July 2003 LiDAR flight error band).

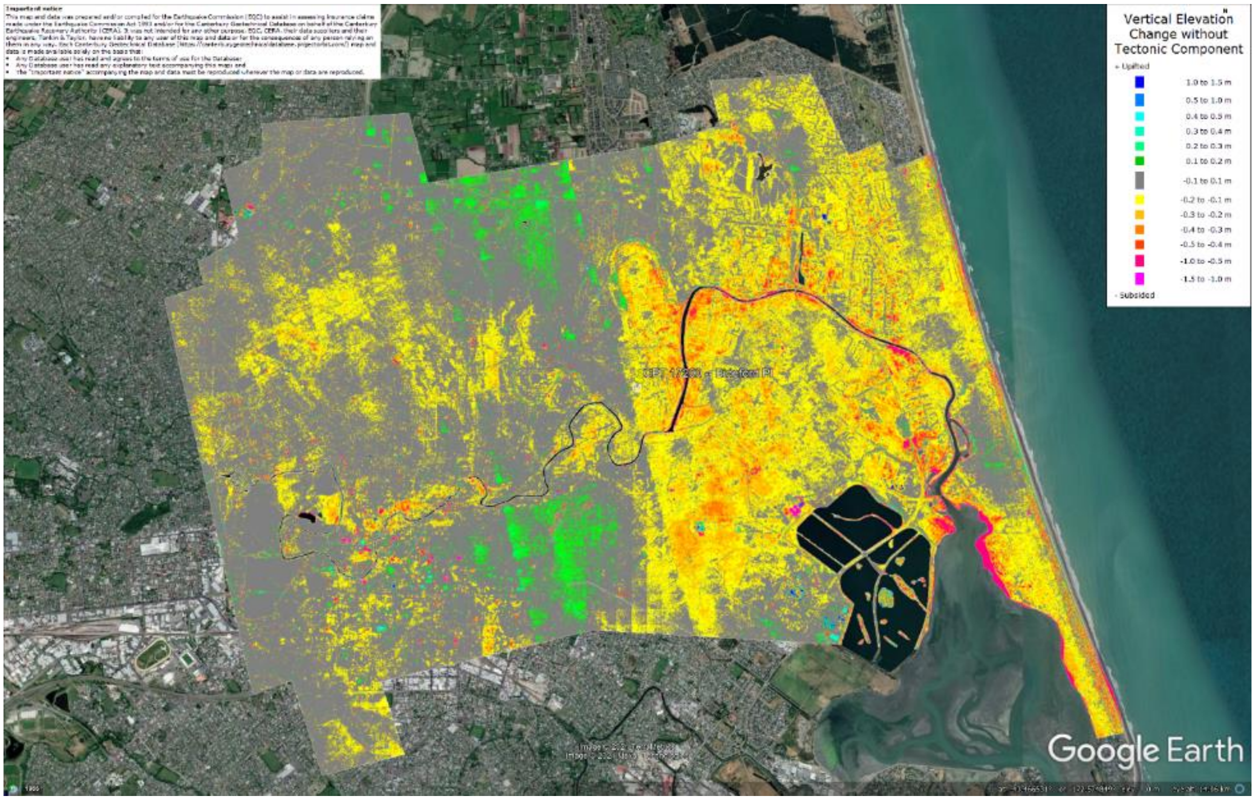

Figure 30: Vertical Ground Movements (Surface – Tectonic) for Feb 2011 Earthquake – the site is not in the apparent zone of underestimated ground surface subsidence.

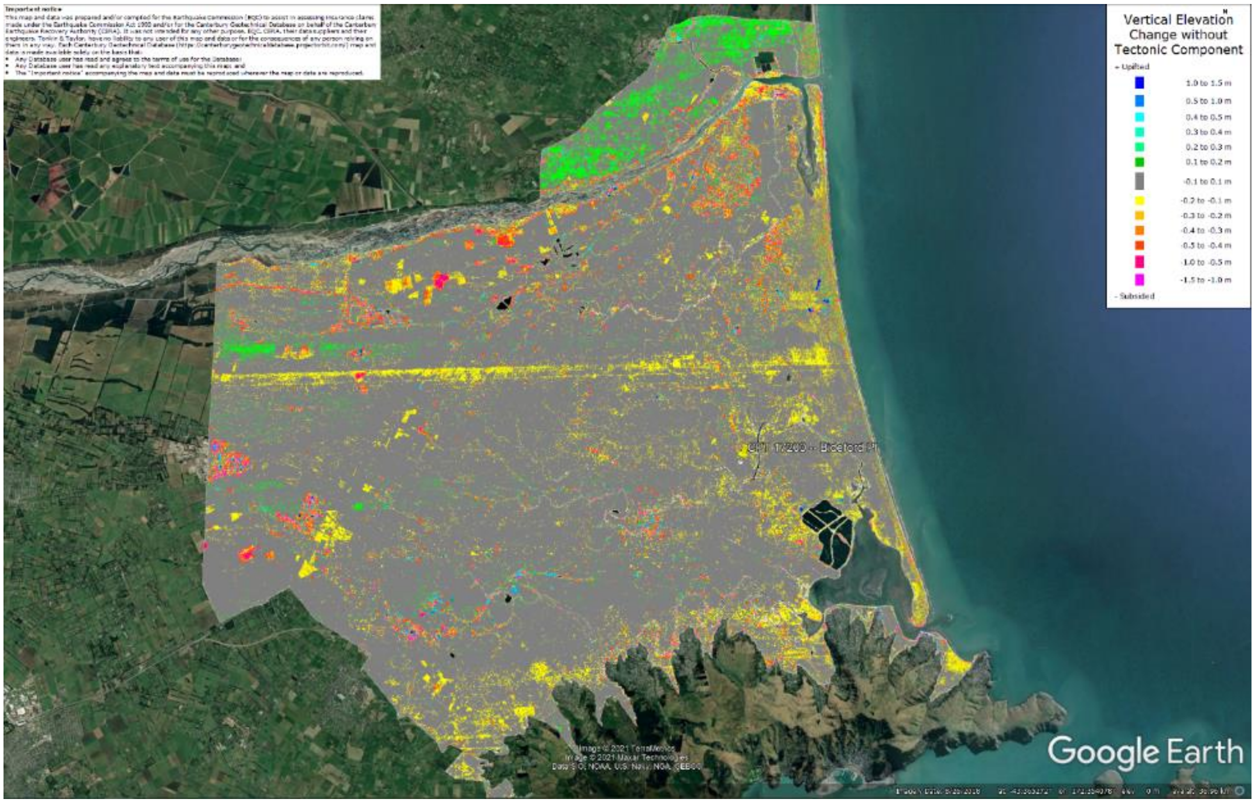

Figure 31: Vertical Ground Movements (Surface – Tectonic) for June 2011 Earthquake – the site is not in the apparent zone of overestimated or underestimated ground surface subsidence.

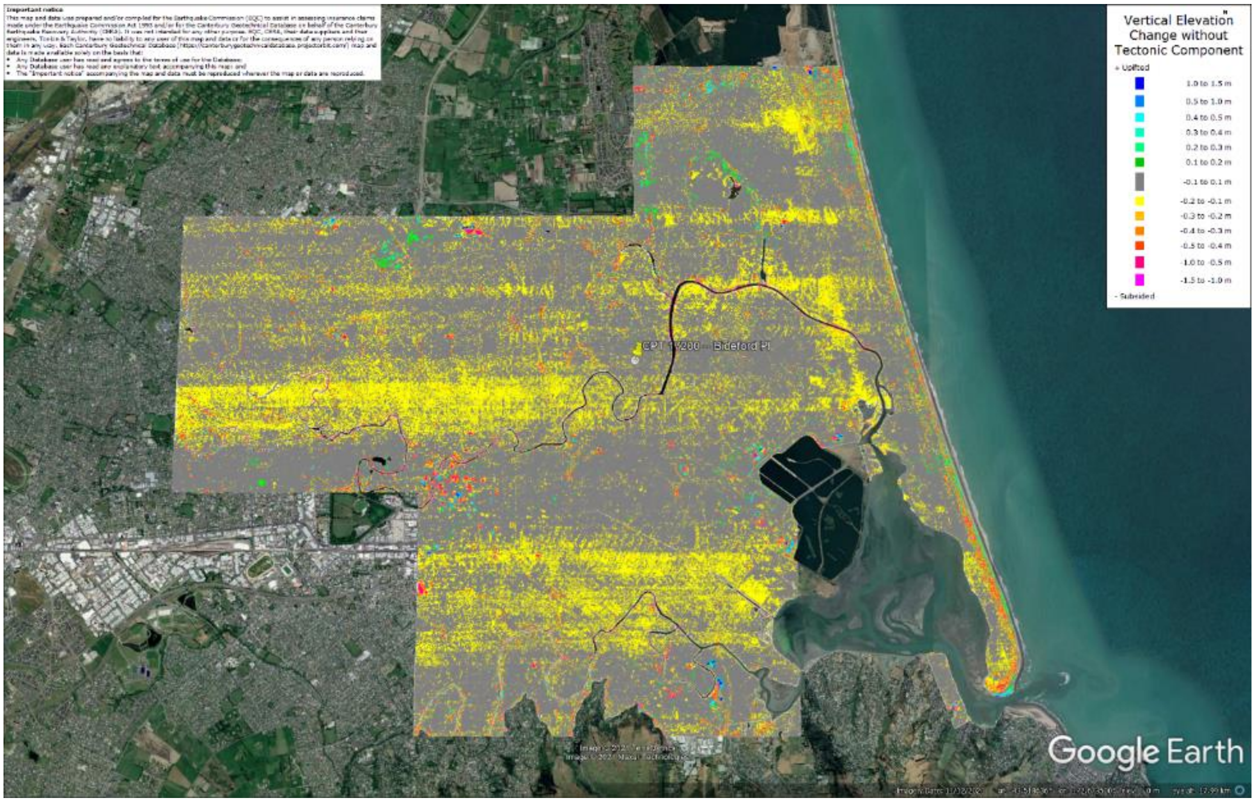

Figure 32: Vertical Ground Movements (Surface – Tectonic) for Dec 2011 Earthquake – the site is not in the apparent zone of overestimated or underestimated ground surface subsidence.

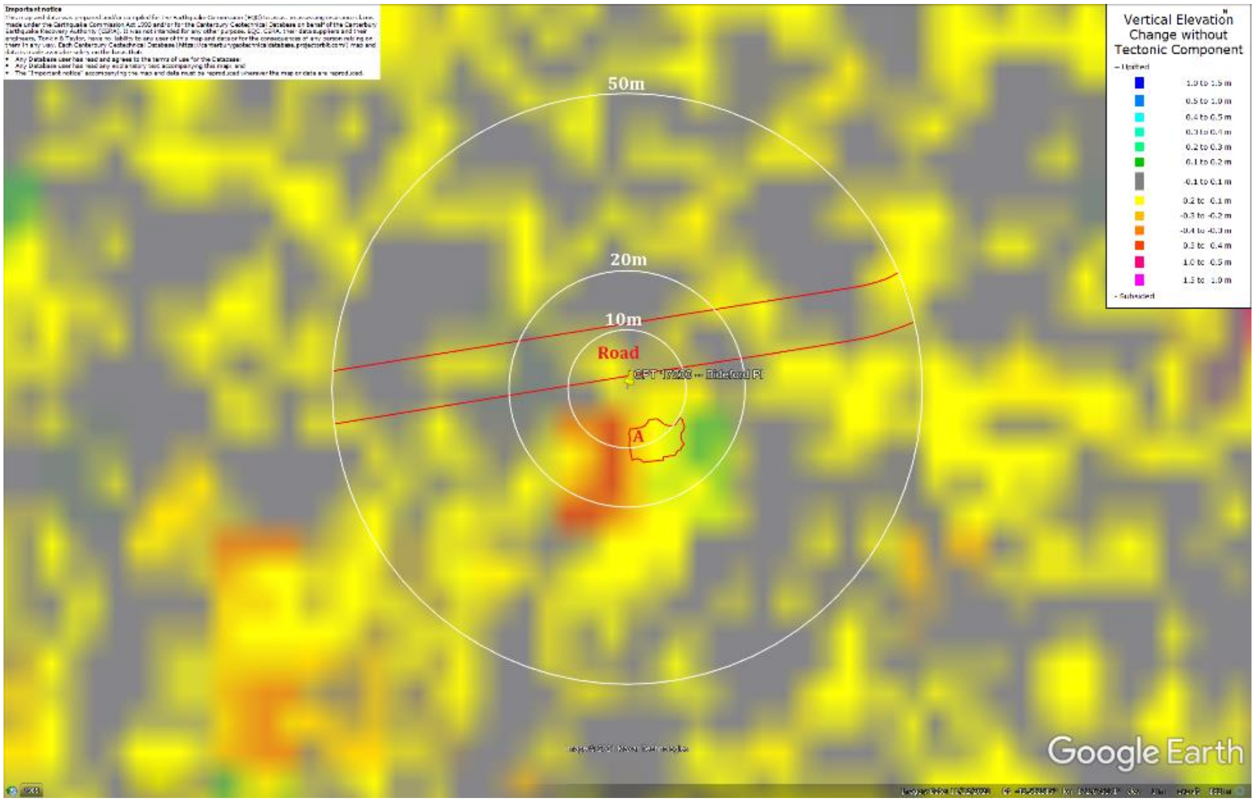

Figure 33: Ground surface subsidence without tectonic component for Sep 2010 Earthquake according to the LiDAR DEM.

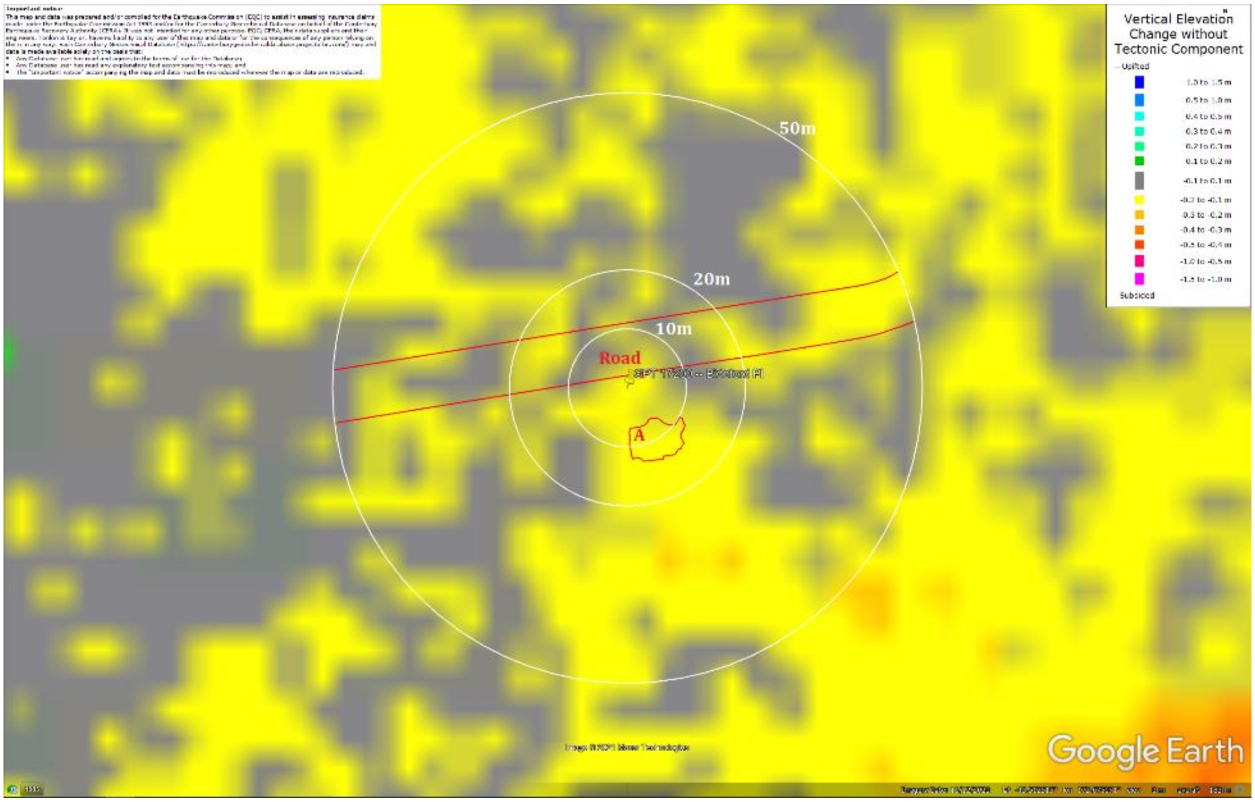

Figure 34: Ground surface subsidence without tectonic component for Feb 2011 Earthquake according to the LiDAR DEM.

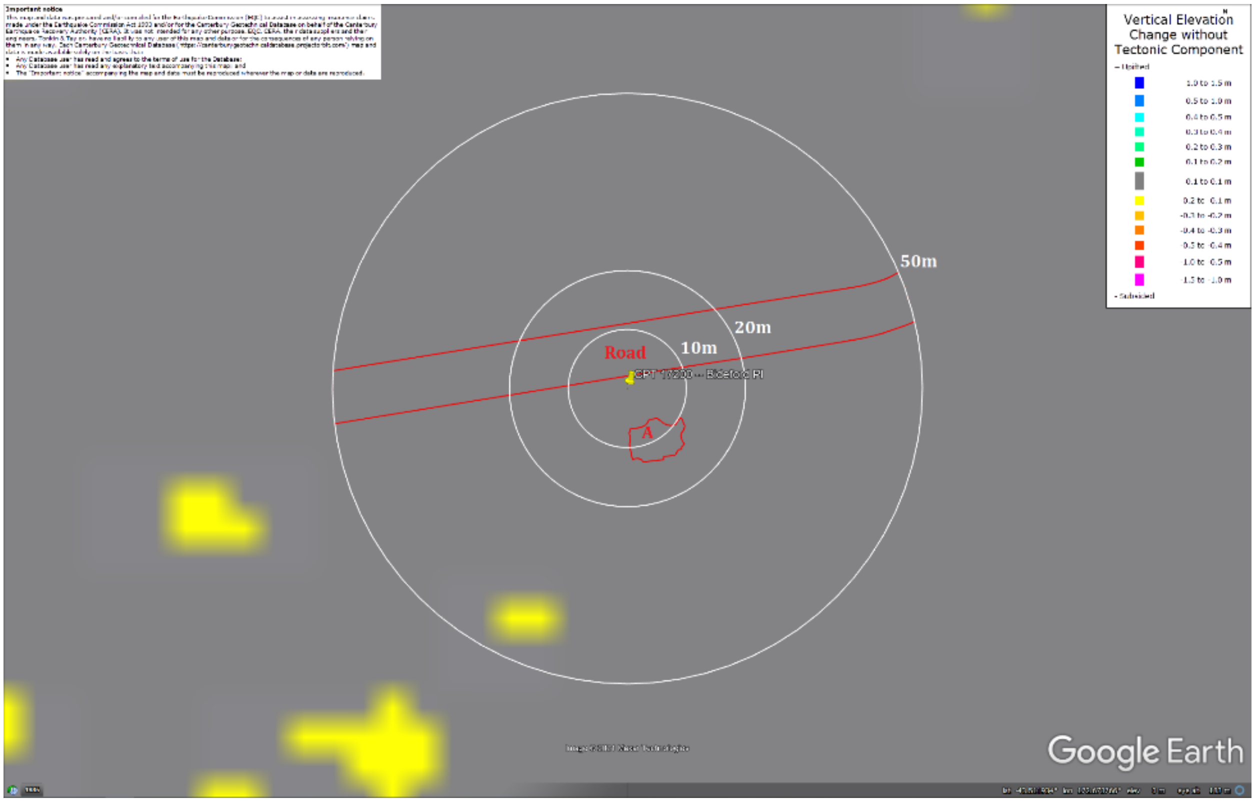

Figure 35: Ground surface subsidence without tectonic component for June 2011 Earthquake according to the LiDAR DEM.

Figure 36: Ground surface subsidence without tectonic component for Dec 2011 Earthquake according to the LiDAR DEM.

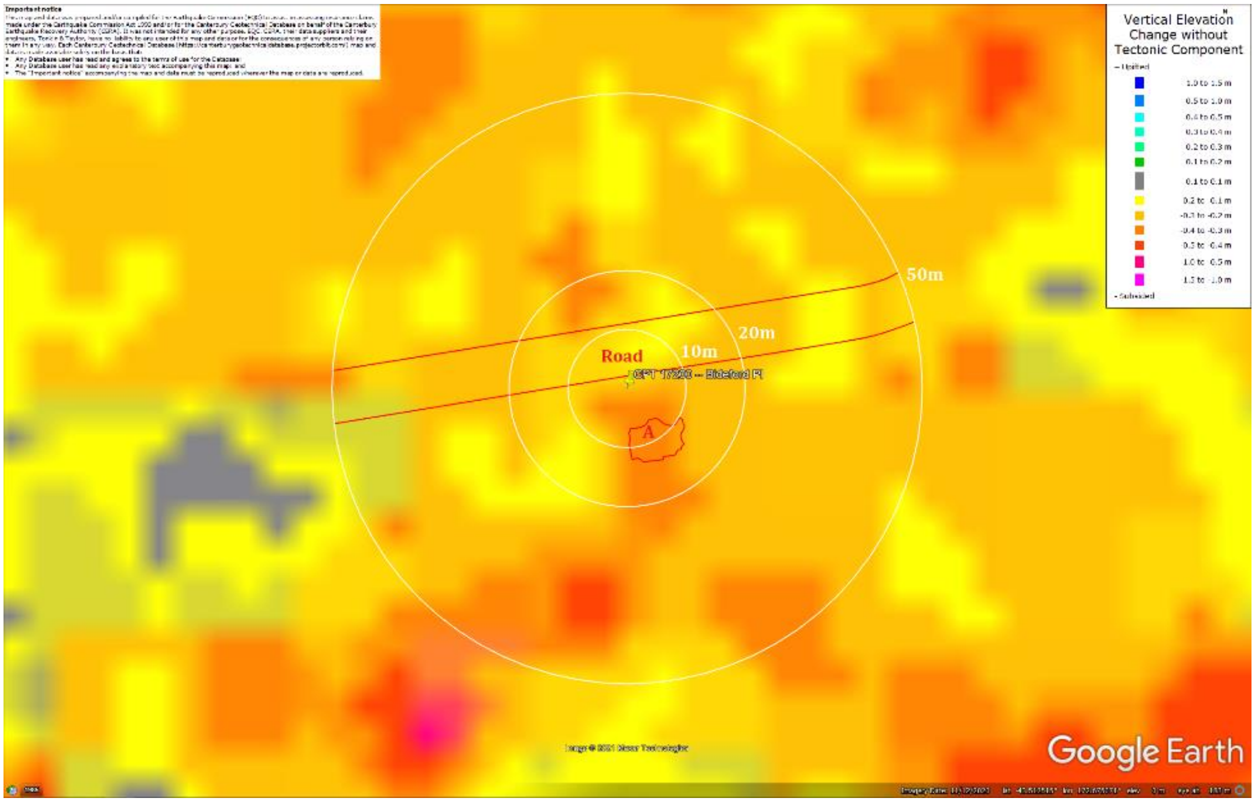

Figure 37: Ground surface subsidence without tectonic component for Canterbury Earthquake Sequence according to the LiDAR DEM.

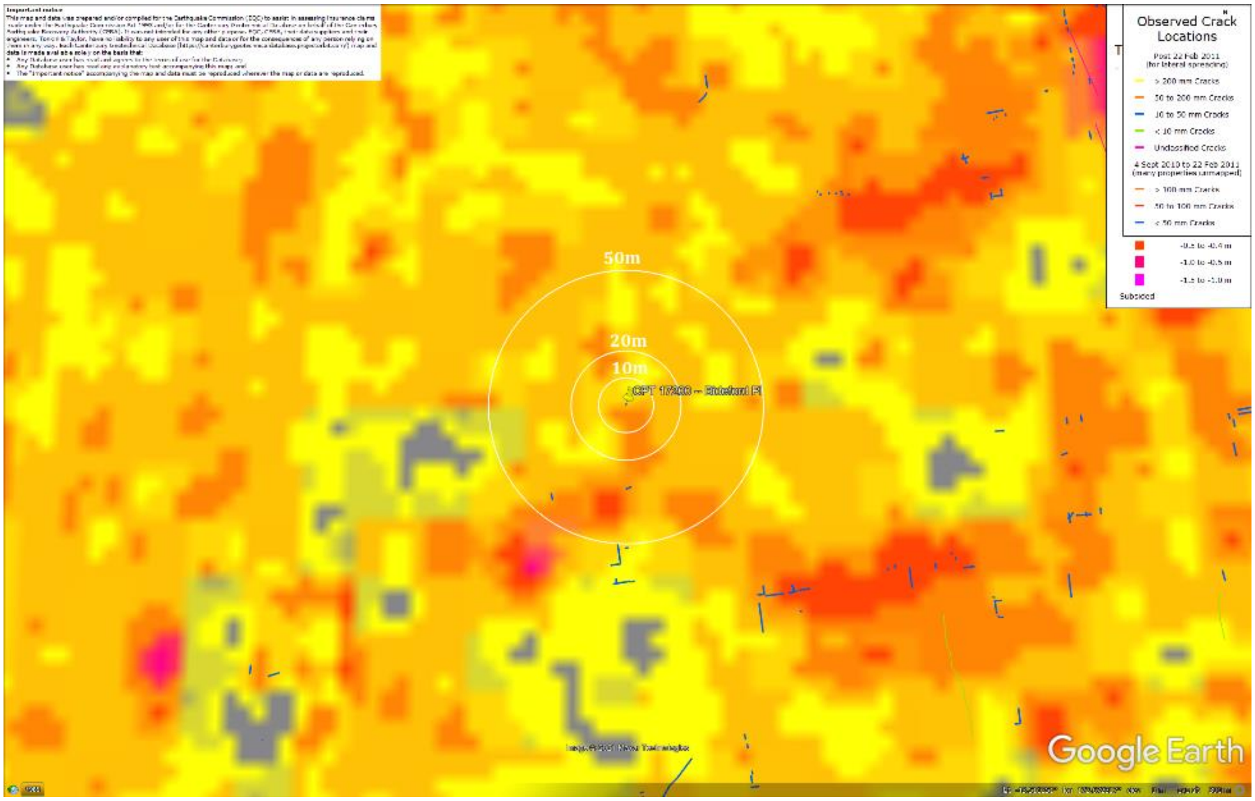

Figure 38: No lateral spreading for Canterbury Earthquake Sequence.

Figure 39: Vertical tectonic movements for Sep 2010 Earthquake.

Figure 40: Vertical tectonic movements for Feb 2011 Earthquake.

Figure 41: Vertical tectonic movements for June 2011 Earthquake.

Figure 42: Vertical tectonic movements for Dec 2011 Earthquake.

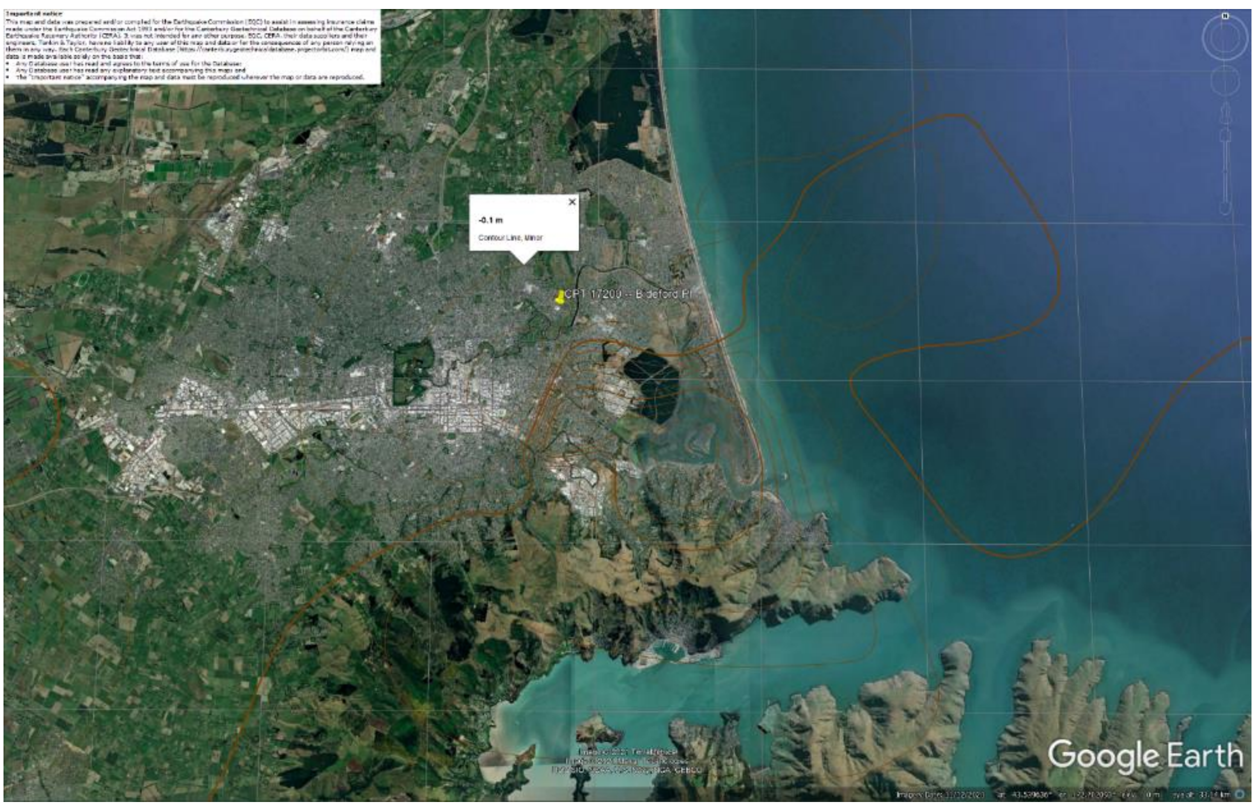

Figure 43: Vertical tectonic movements for Canterbury Earthquake Sequence.

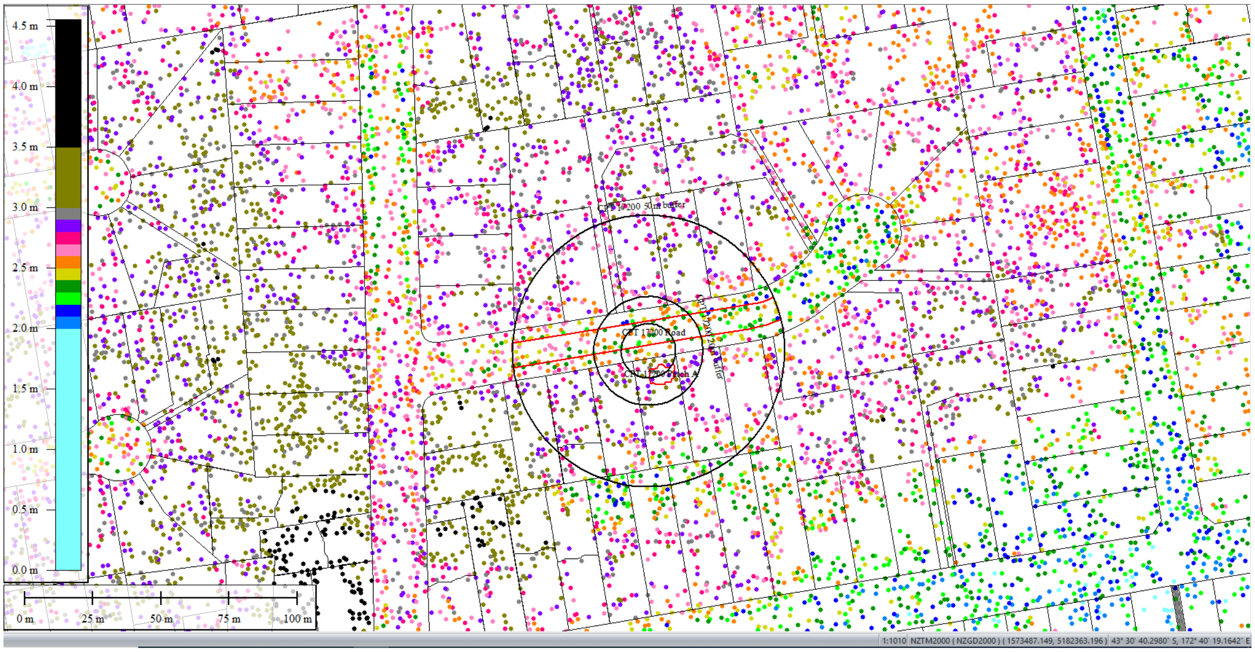

Figure 44: Jul 2003 LiDAR survey.

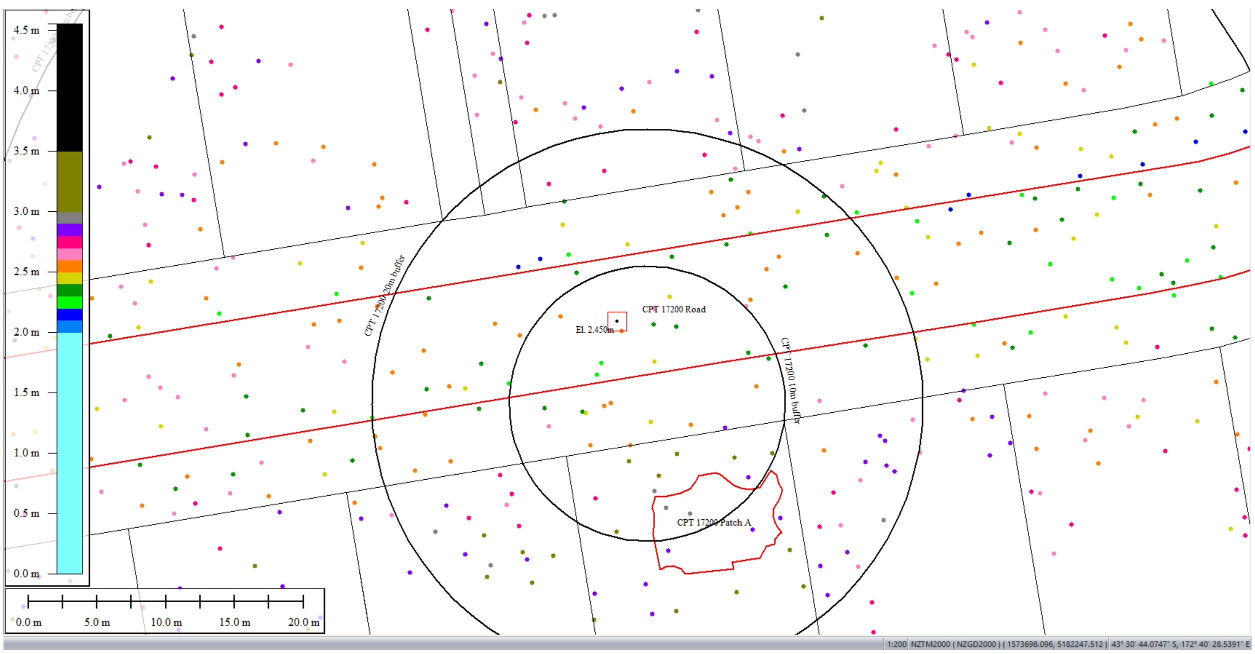

Figure 45: Ground surface elevation averaged over 20-m buffer for Road for Jul 2003 LiDAR survey.

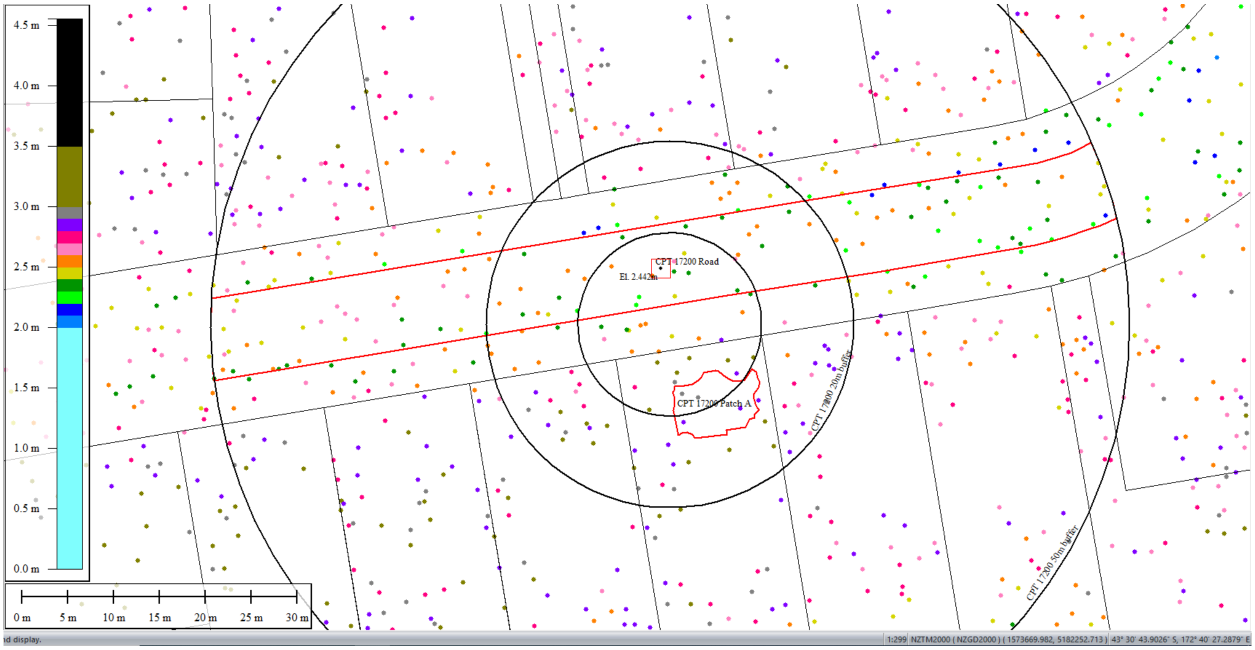

Figure 46: Ground surface elevation averaged over 50-m buffer for Road for Jul 2003 LiDAR survey.

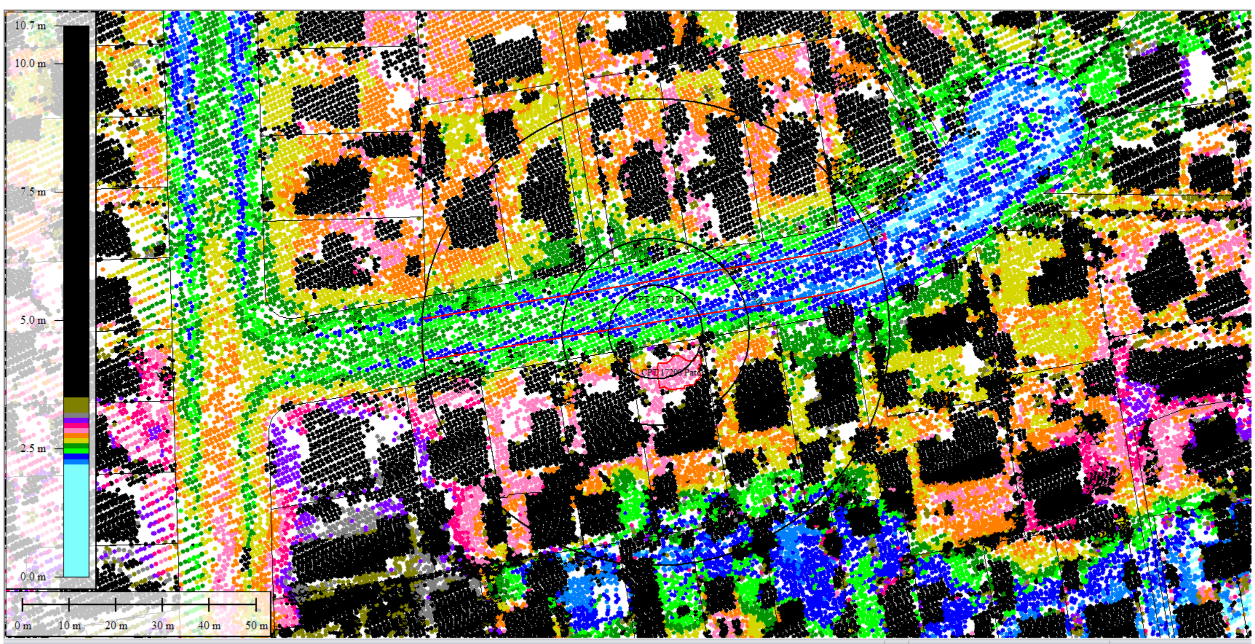

Figure 47: Sep 5, 2010 LiDAR survey.

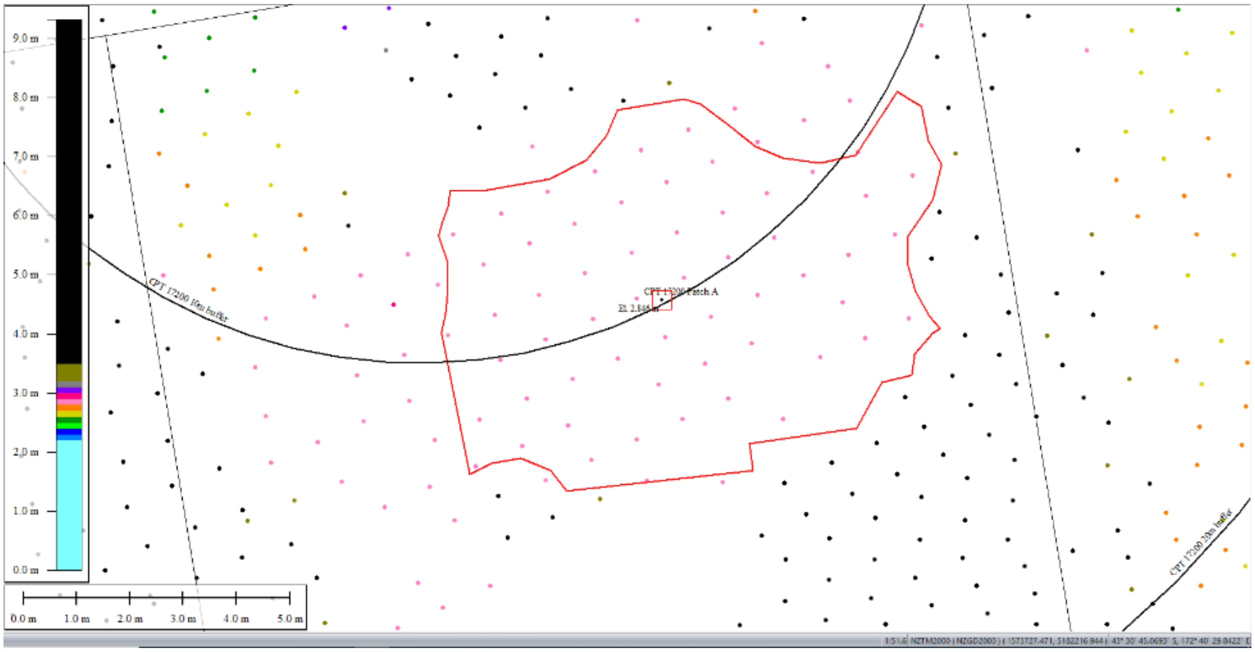

Figure 48: Ground surface elevation averaged over 10-m, 20-m, and 50-m buffers for Patch A for Sep 5, 2010 LiDAR survey.

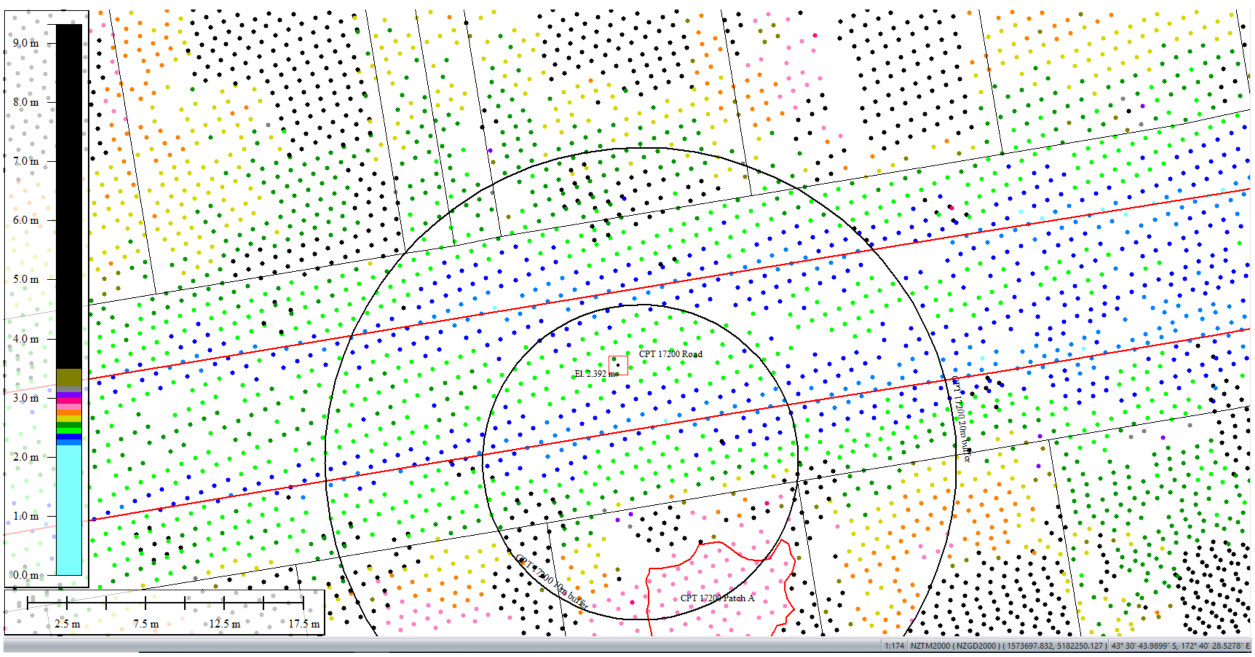

Figure 49: Ground surface elevation averaged over 20-m buffer for Road for Sep 5, 2010 LiDAR survey.

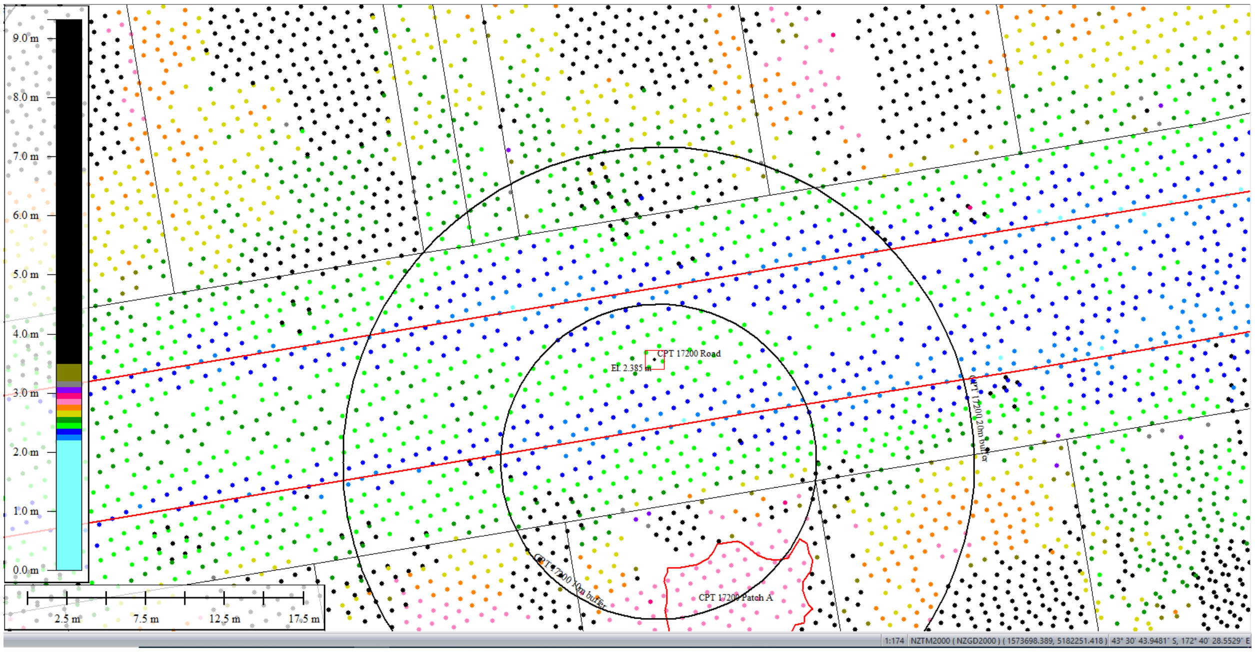

Figure 50: Ground surface elevation averaged over 50-m buffer for Road for Sep 5, 2010 LiDAR survey.

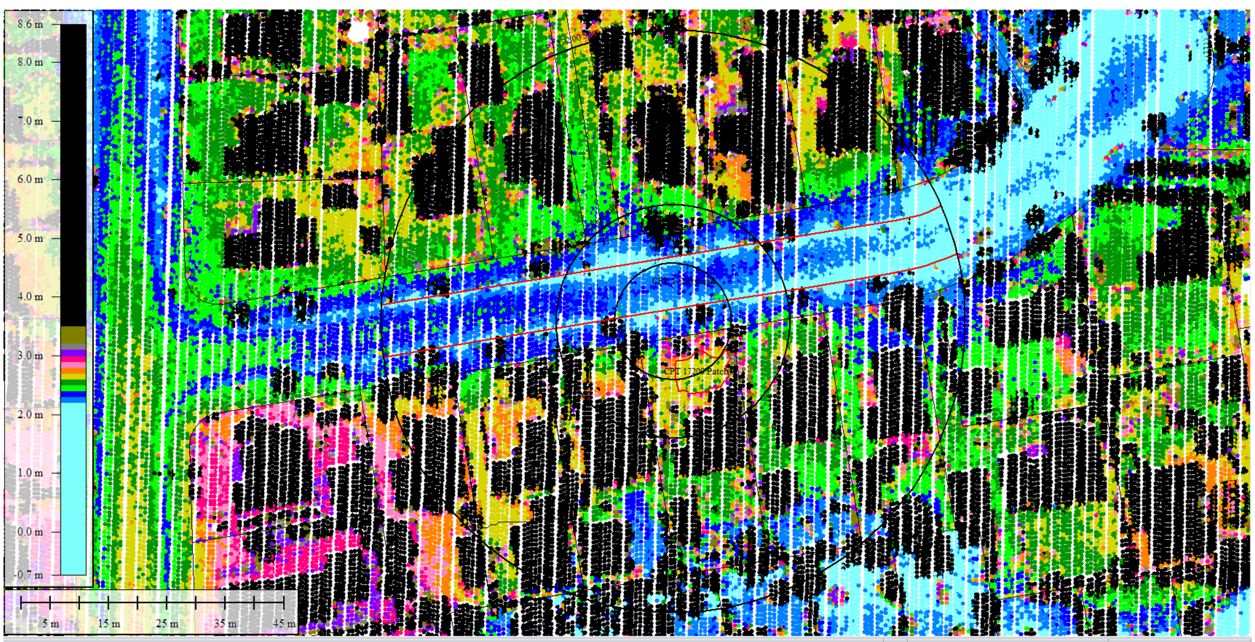

Figure 51: Mar 2011 LiDAR survey.

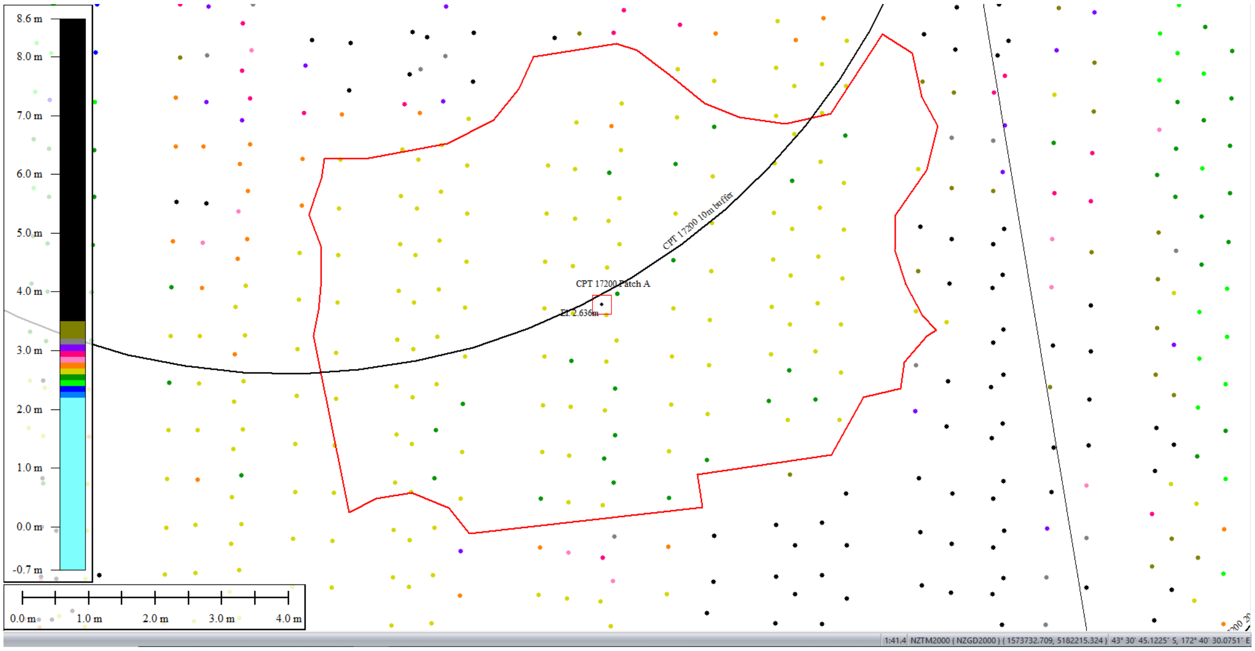

Figure 52: Ground surface elevation averaged over 10-m, 20-m, and 50-m buffers for Patch A for Mar 2011 LiDAR survey.

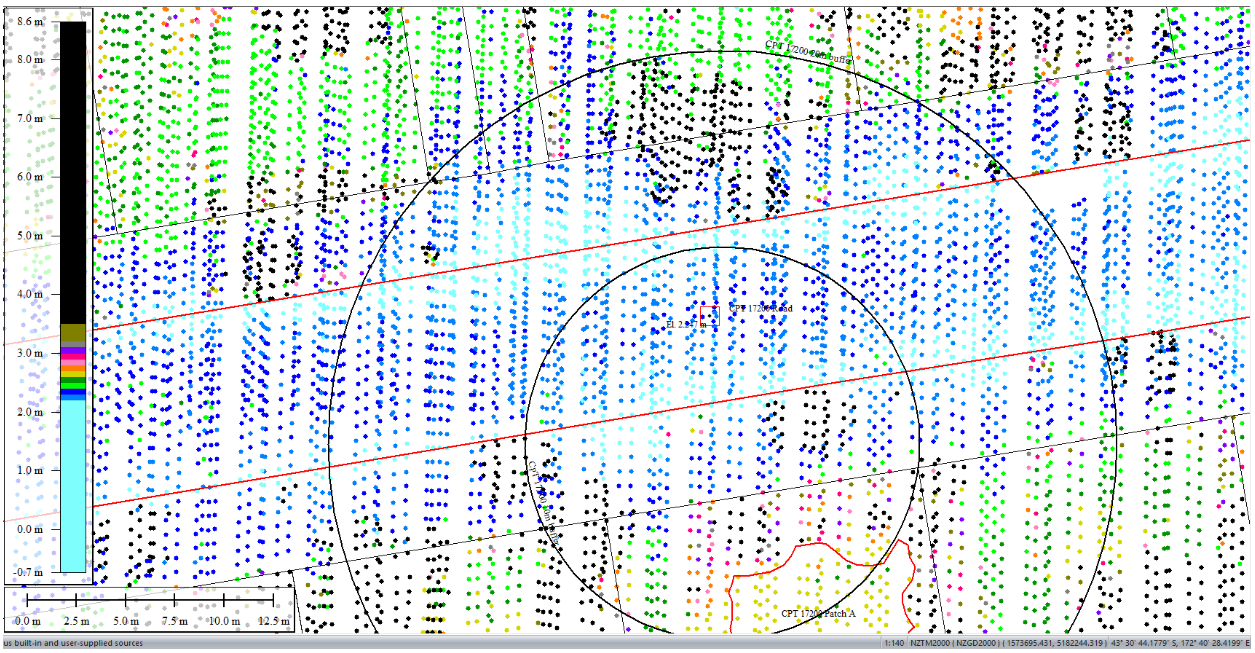

Figure 53: Ground surface elevation averaged over 20-m buffer for Road for Mar 2011 LiDAR survey.

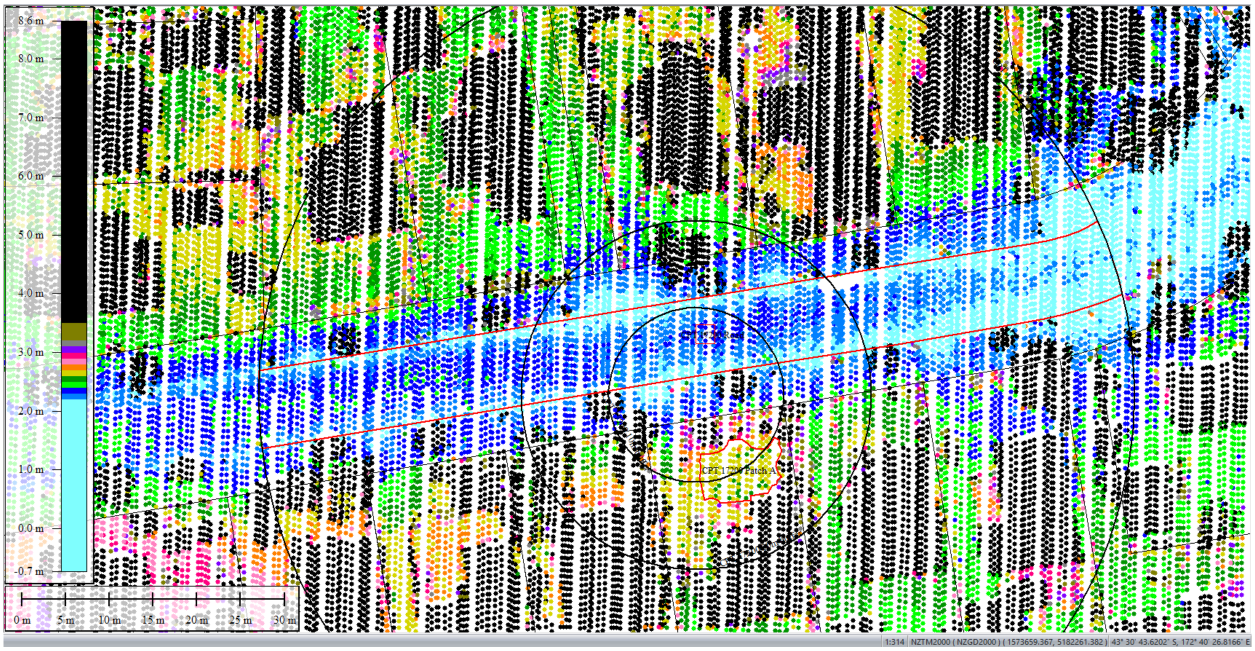

Figure 54: Ground surface elevation averaged over 50-m buffer for Road for Mar 2011 LiDAR survey (el. 2.237m).

Figure 55: May 2011 LiDAR survey.

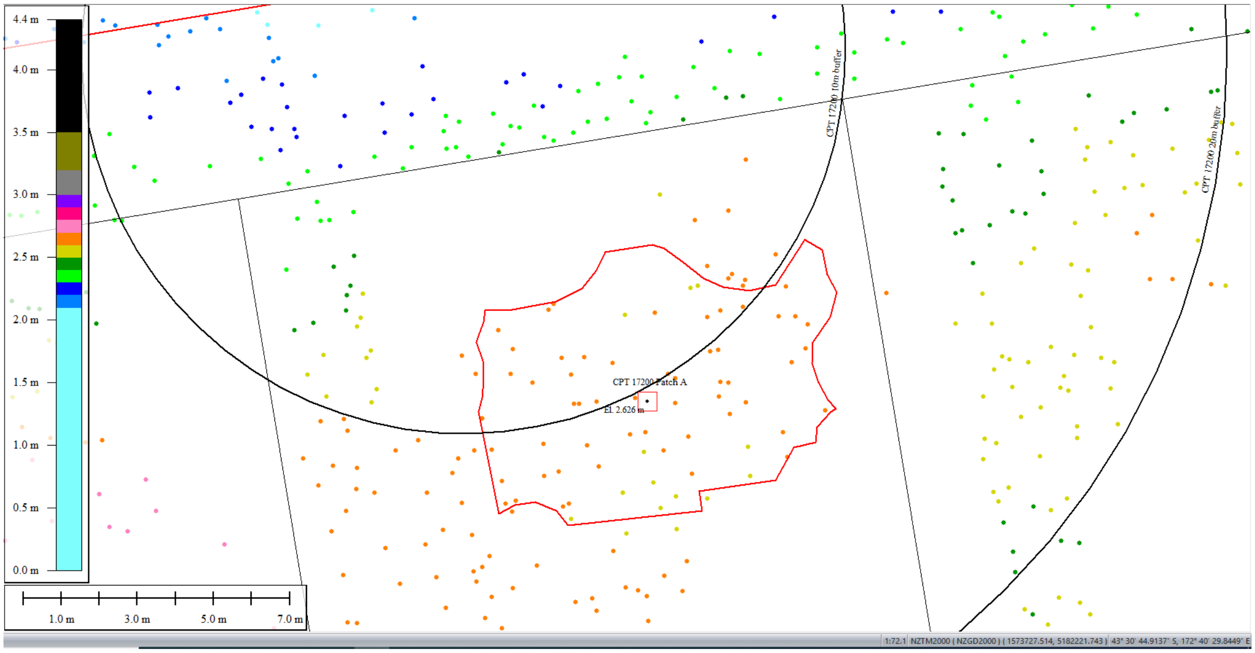

Figure 56: Ground surface elevation averaged over 10-m, 20-m, and 50-m buffers for Patch A for May 2011 LiDAR survey.

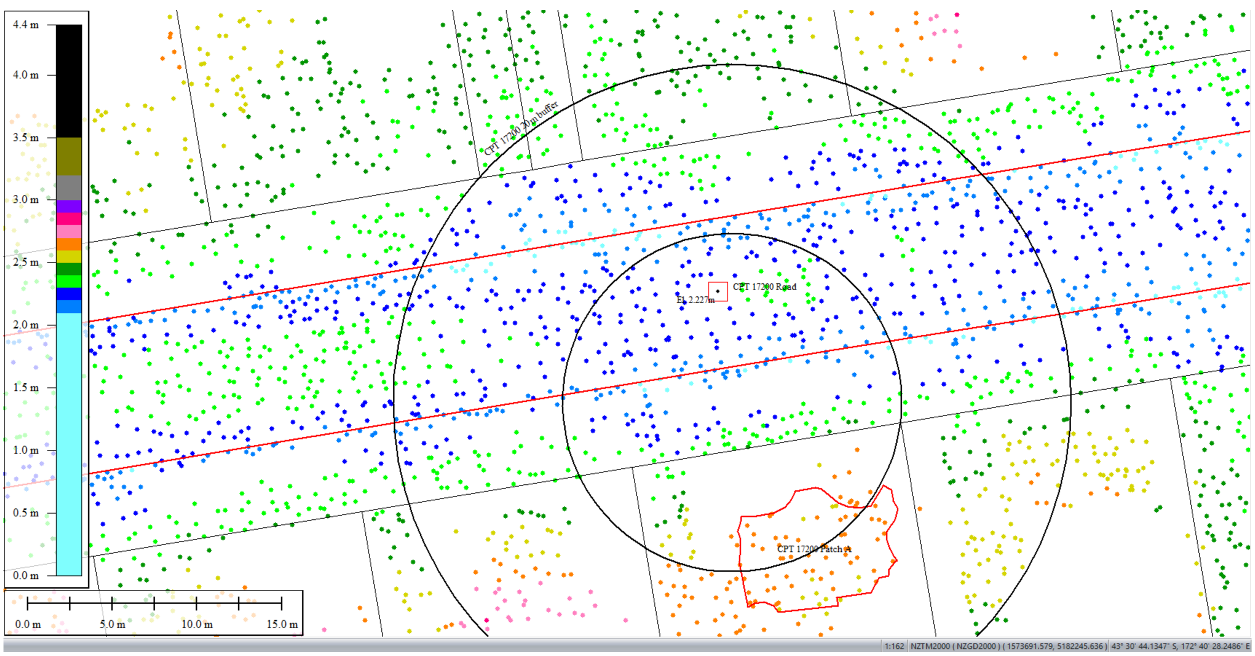

Figure 57: Ground surface elevation averaged over 20-m buffer for Road for May 2011 LiDAR survey.

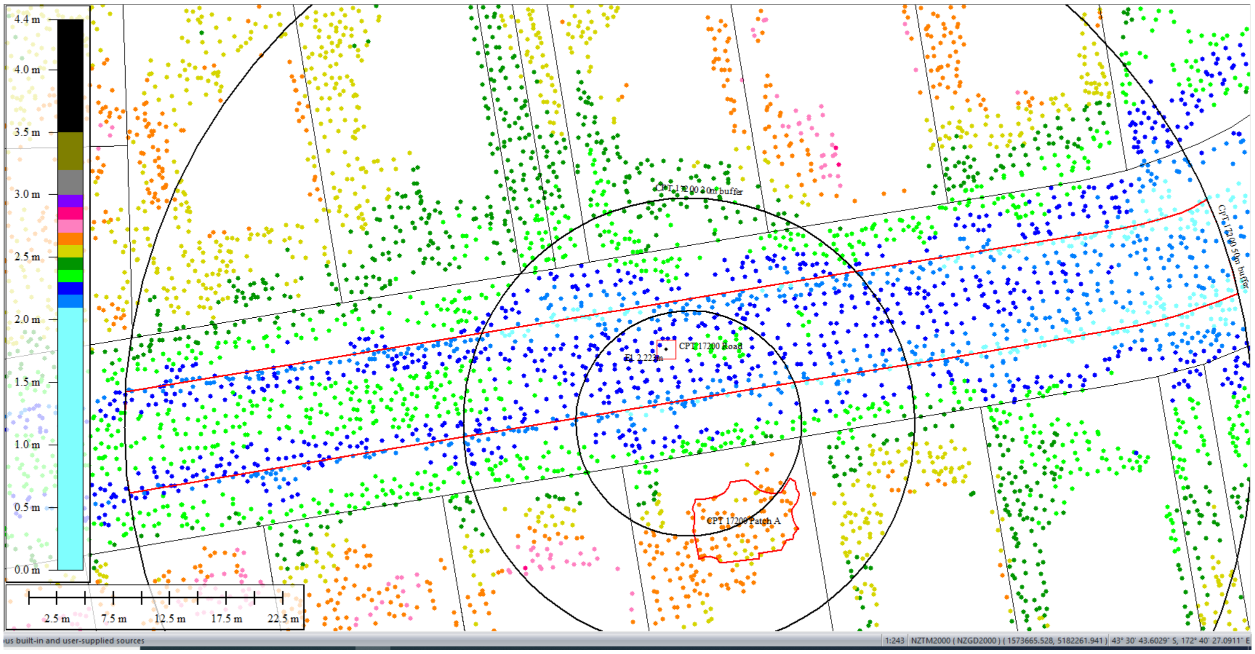

Figure 58: Ground surface elevation averaged over 50-m buffer for Road for May 2011 LiDAR survey.

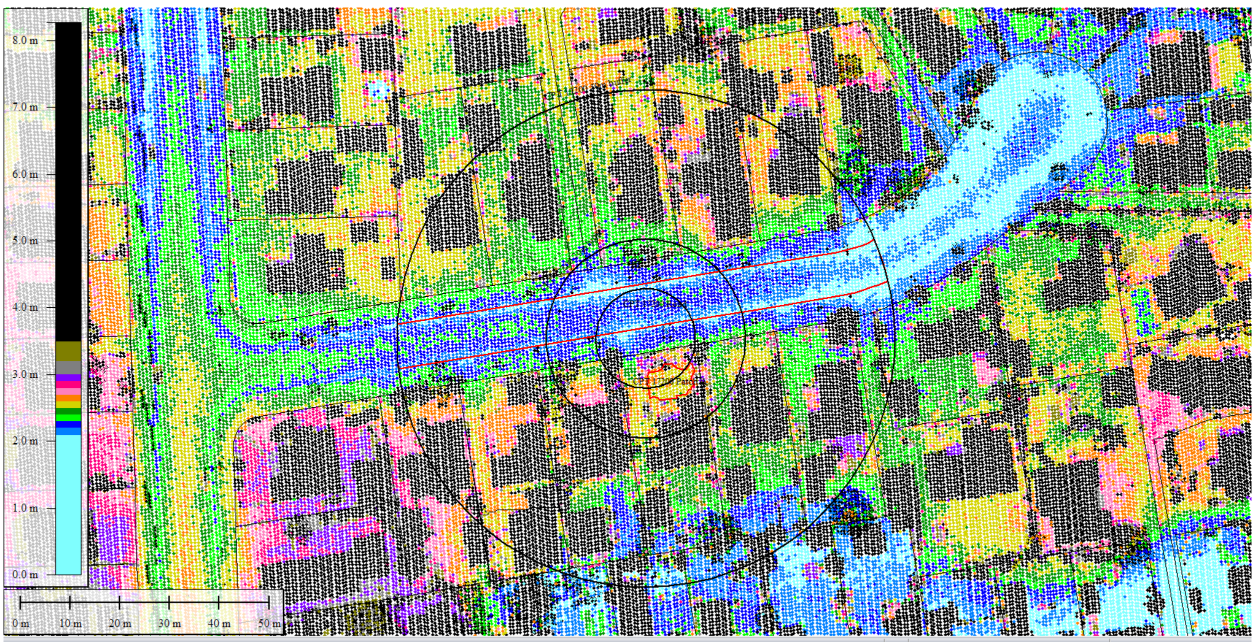

Figure 59: Sep 2011 LiDAR survey.

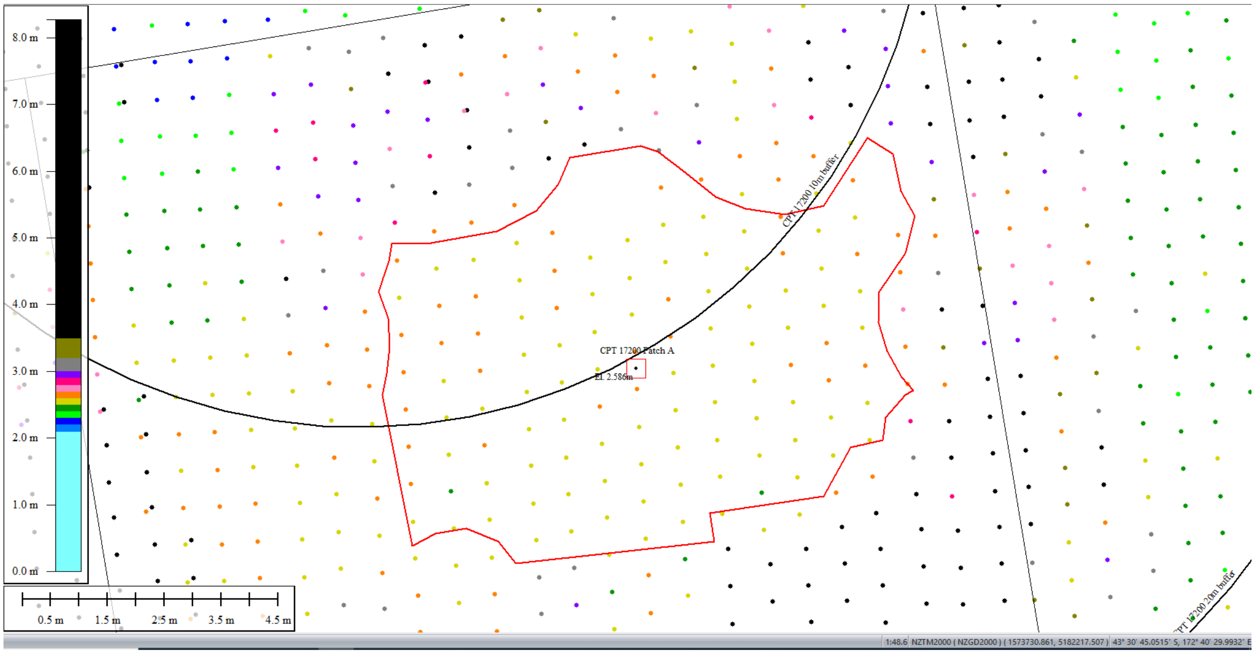

Figure 60: Ground surface elevation averaged over 10-m, 20-m, and 50-m buffers for Patch A for Sep 2011 LiDAR survey.

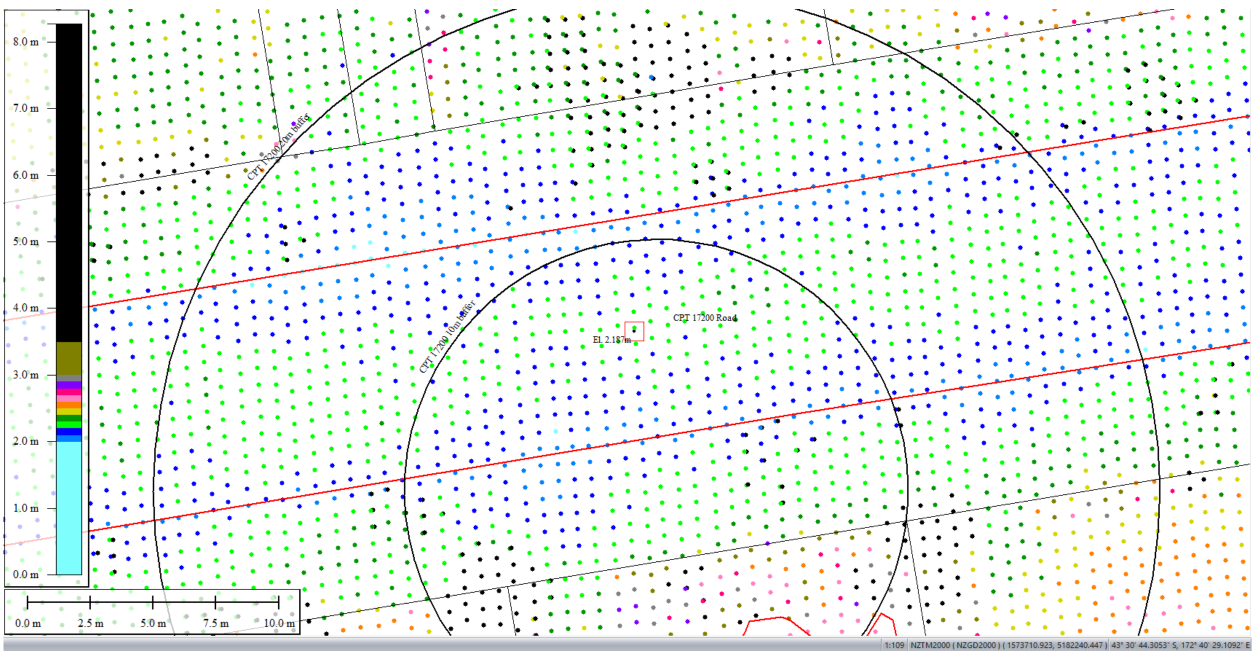

Figure 61: Ground surface elevation averaged over 20-m buffer for Road for Sep 2011 LiDAR survey.

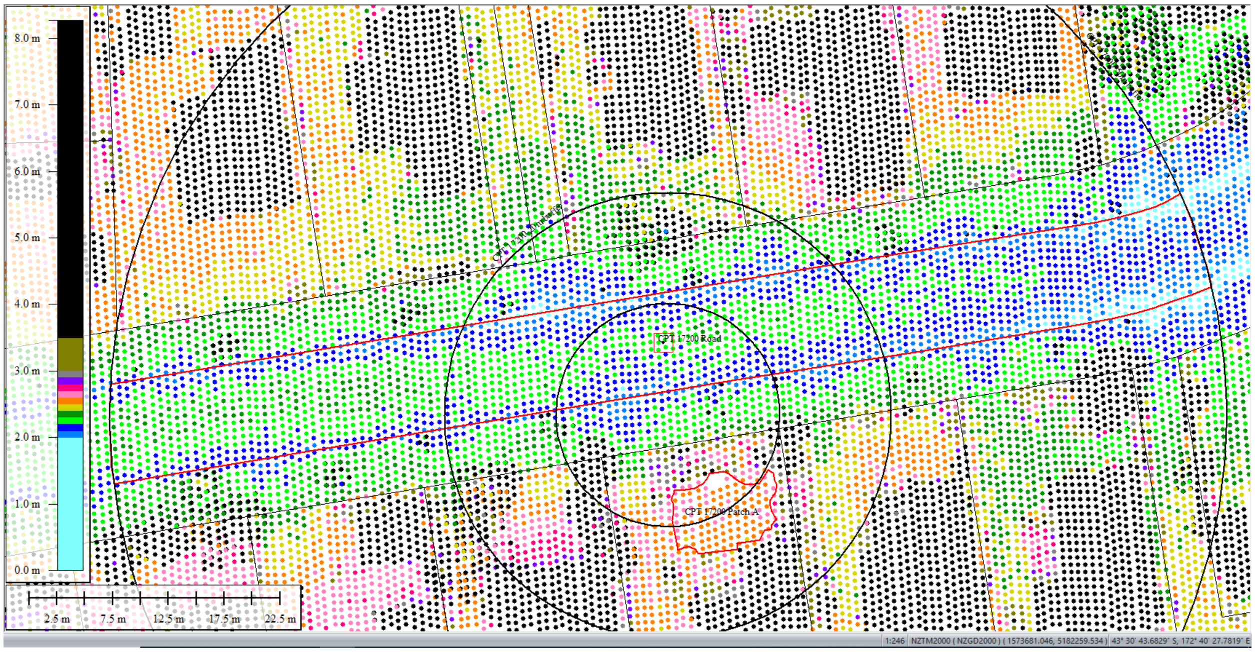

Figure 62: Ground surface elevation averaged over 50-m buffer for Road for Sep 2011 LiDAR survey (el. 2.181m).

Figure 63: Aerial photograph showing the ejecta outline at the site for Sep-10 EQ.

Figure 64: Aerial photograph showing the ejecta outline at the site for Feb-11 EQ.

Figure 65: Aerial photograph acquired on 16 Jun 2011 showing the ejecta outline at the site for Jun-11 EQ.

Contents of this figure cannot be shared as doing so is restricted by a Non-Disclosure Agreement.

Figure 66: LDAT inspection notes for the property with Patch A (inspection date: 16 June 2011).

Figure 67: Ground photographs showing ejecta remnants at the property with Patch A (photograph date: 16 June 2011).

Figure 68: Ground photographs showing ejecta remnants at the properties within the 50-m buffer (photograph date: 16 June 2011).

Figure 69: PGA for Sep-10 EQ (st. dev. = 0.275-0.325 ln units).

Figure 70: PGA for Feb-11 EQ (st. dev. = 0.300-325 ln units).

Figure 71: PGA for Jun-11 EQ (st. dev. = 0.325-0.350 ln units).

Figure 72: PGA for Dec-11 EQ (st. dev. = 0.350-0.375 ln units).

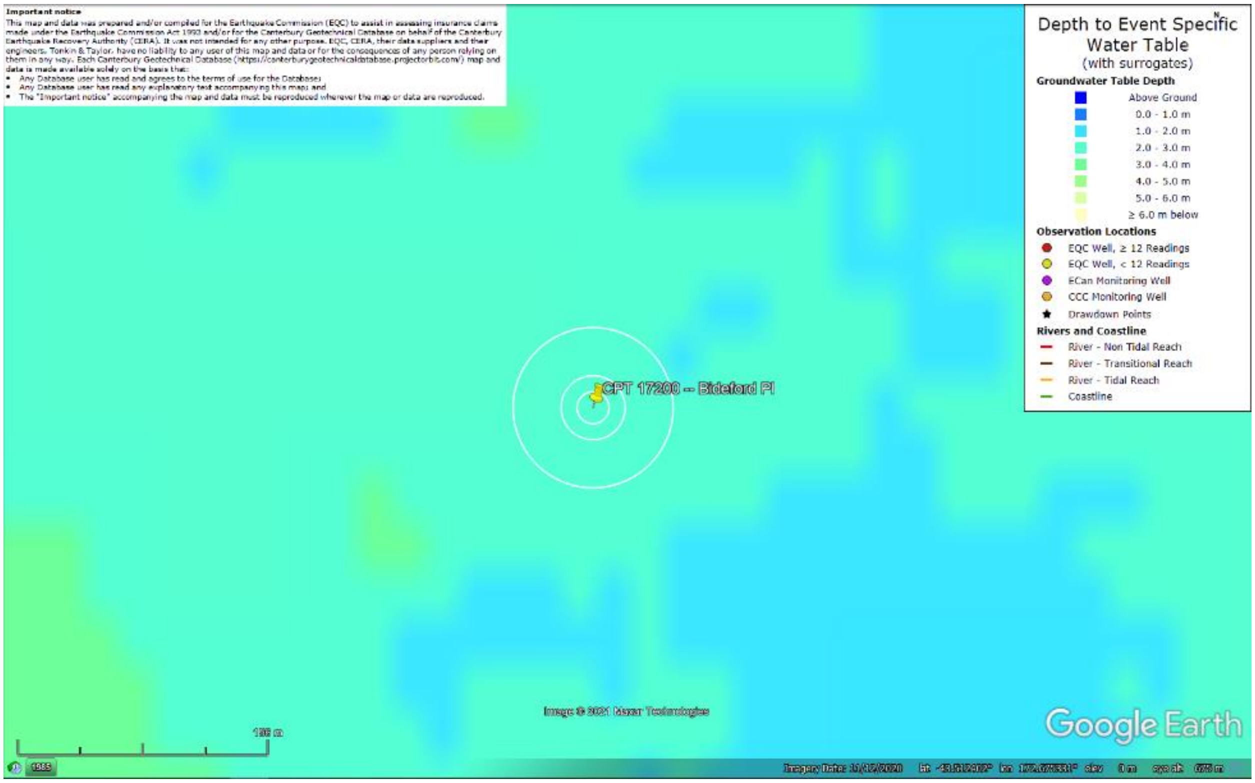

Figure 73: Depth to groundwater table for Sep-10 EQ.

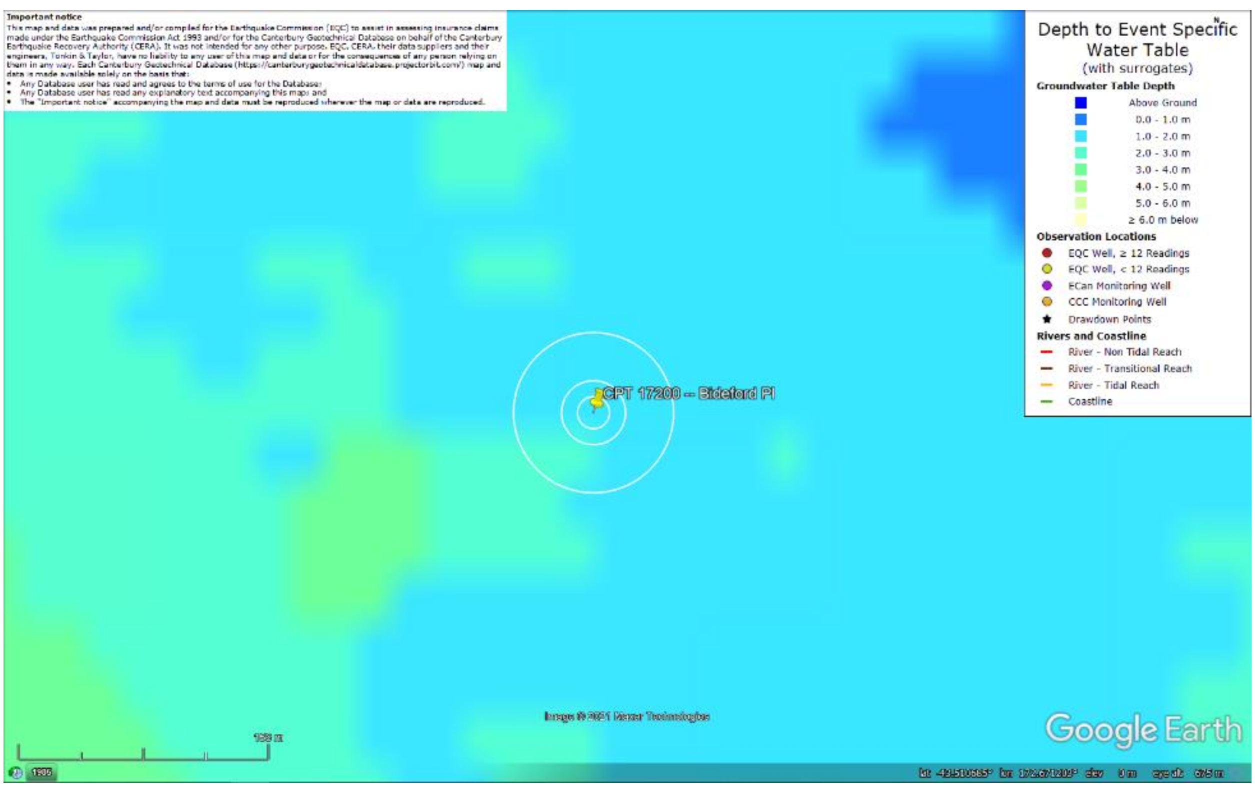

Figure 74: Depth to groundwater table for Feb-11 EQ.

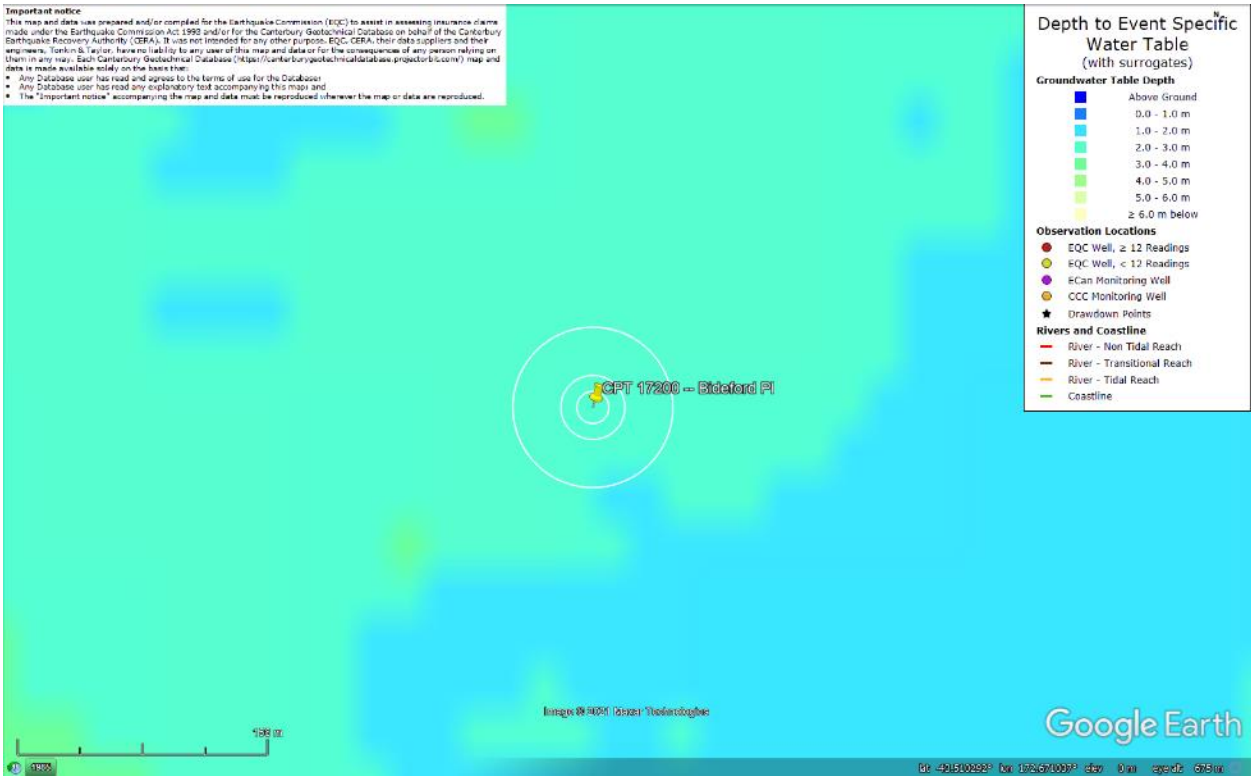

Figure 75: Depth to groundwater table for Jun-11 EQ.

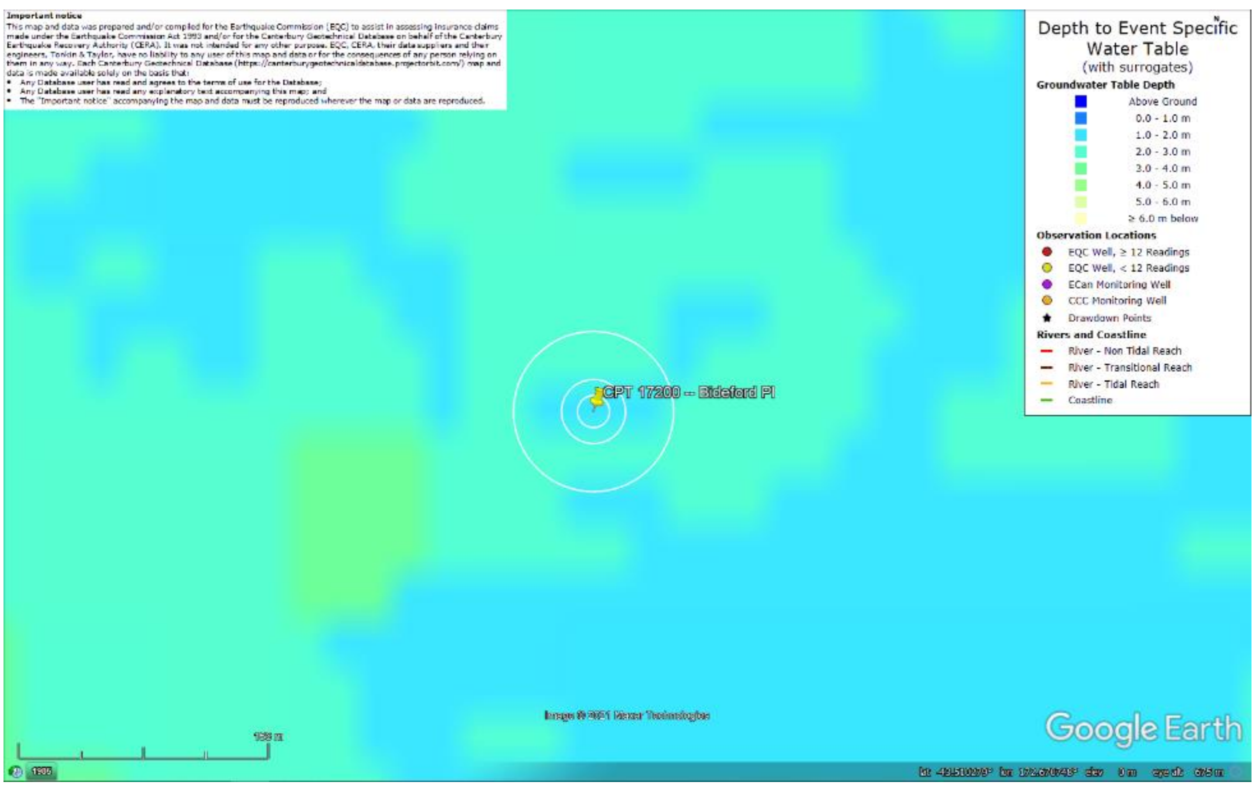

Figure 76: Depth to groundwater table for Dec-11 EQ.

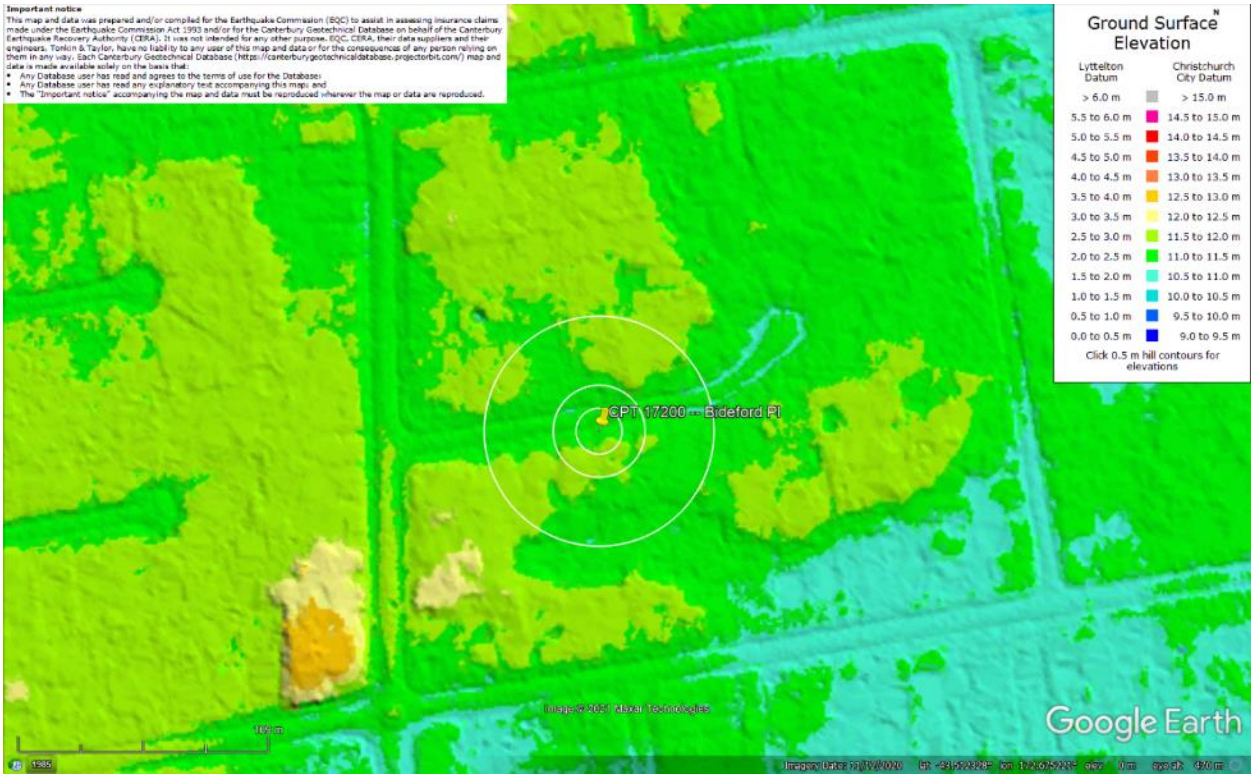

Figure 77: Ground surface elevation according to the Sep-2011 LiDAR survey.

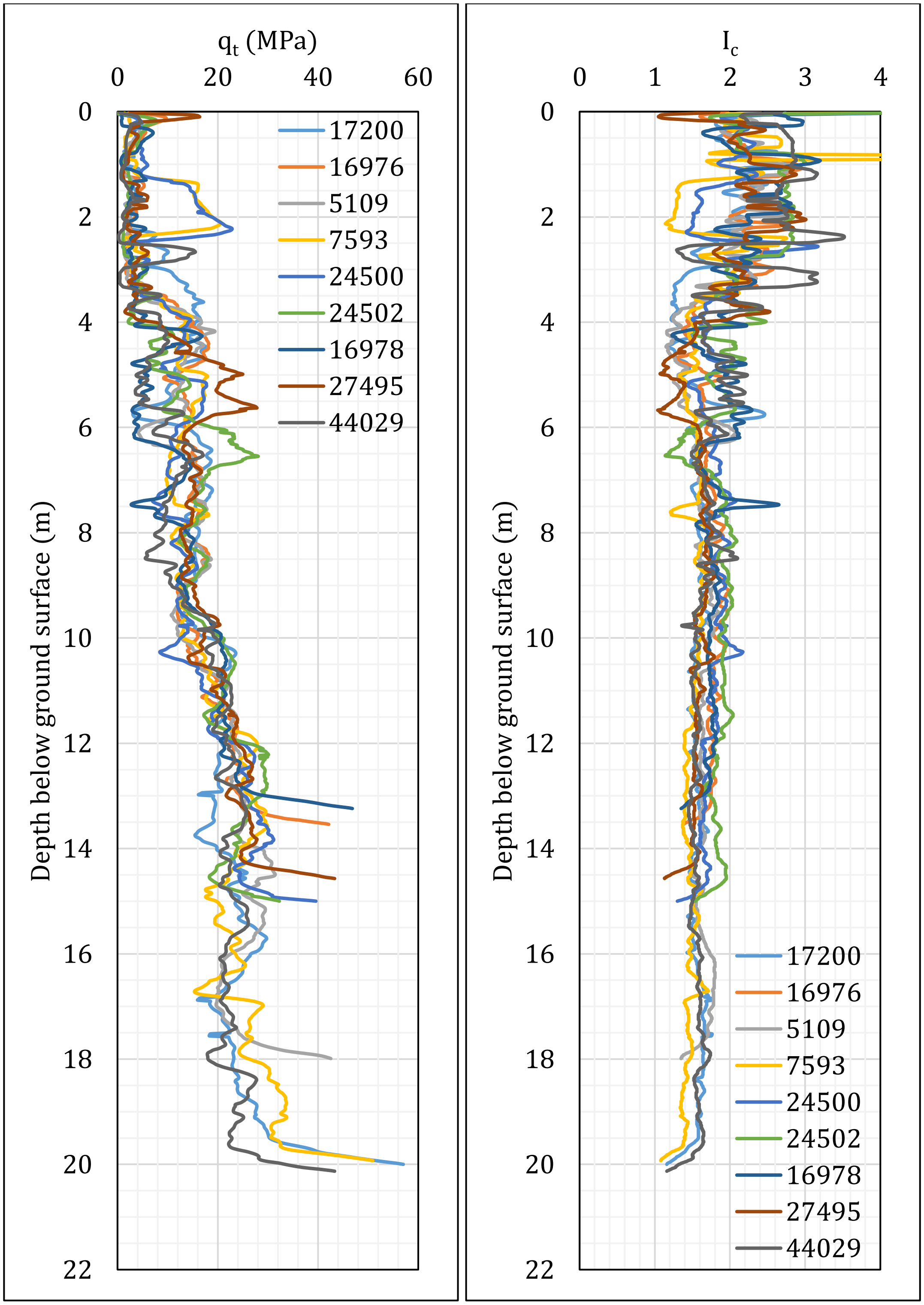

Figure 78: q_t and I_c profiles.

Note 6: The selection of CPTs for the area considered for settlement assessment (Figure 1) is based on the proximity of the CPTs to the considered areas. In accordance with that, the following table shows CPTs that were used for the volumetric settlement analysis in *Cliq v.3.0.3.2*, a CPT soil liquefaction software developed by GeoLogismiki. (The average volumetric settlements were reported in Table 8.)

Table 12: CPT profiles used in volumetric settlement analysis for areas selected for settlement assessment.

CPT ID No.	Patch A	Road (20-m buffer)	Road (50-m buffer)
17200		✓	✓
16976	✓		
5109	✓		
7593			
24500		✓	✓
24502			
16978			
27495			
44029			✓

Note: CPT 17200 was used to compute the volumetric settlement for CPTs 16976, 5109, 24500, 24502, 1678, and 27495 for the respective depth ranges: 13.5-20 m, 17.8-20m, 15-20m, 15-20m, 13.2-20m, and 14.6-20m.

Table 13: CPT-based results.

		CPT ID								
EQ Event	Parameter	17200	16976	5109	7593	24500	24502	16978	27495	44029
Sep-10	S_{V1D} (mm)	2	3	3	5	0	2	10	2	9
	LSN	0	1	1	1	0	0	2	1	1
	LPI	0	0	0	0	0	0	0	0	0
	LPI_{ish}	0	0	0	0	0	0	0	0	0
	$D_{FS<1}$ (m)	undet.	undet.	undet.	undet.	undet.	undet.	undet.	undet.	undet.
Feb-11	S_{V1D} (mm)	47	41	60	84	28	29	99	38	104
	LSN	13	15	19	16	7	8	24	12	19
	LPI	4	6	8	9	3	4	13	5	13
	LPI_{ish}	3	5	7	6	2	1	9	3	6
	$D_{FS<1}$ (m)	1.78	1.75	1.99	2.55	2.85	2.74	2.02	2.54	3.34
Jun-11	S_{V1D} (mm)	5	9	10	14	3	5	28	7	24
	LSN	1	3	3	3	1	1	6	2	4
	LPI	0	0	0	0	0	0	1	0	0
	LPI_{ish}	0	0	0	0	0	0	0	0	0
	$D_{FS<1}$ (m)	undet.	2.89	undet.	undet.	undet.	undet.	5.57	undet.	undet.
Dec-11	S_{V1D} (mm)	10	22	29	27	6	10	45	13	41
	LSN	2	8	10	6	2	3	10	4	7
	LPI	0	1	1	1	0	0	2	1	1
	LPI_{ish}	0	0	0	1	0	0	0	1	0
	$D_{FS<1}$ (m)	5.64	2.52	2.48	2.95	undet.	3.69	3.53	3.58	5.07

Notes: $D_{FS<1}$ = Depth to the first liquefiable layer (FS_L<1) that is at least 200-mm thick, as determined by the Boulanger and Idriss (2016) liquefaction-triggering procedure (P_L=50%, C_{FC}=0.13, and $I_{c,cutoff}$ =2.6), and exported from *Cliq v.3.0.3.2*; undet. = the specified soil layer was not detected.

Table 13 (continued): CPT-based results.

EQ Event	Parameter	CPT ID Δ_{16976}	Δ_{5109}	Δ_{24500}	Δ_{24502}	Δ_{16978}	Δ_{27495}
Sep-10	S_{V1D} (mm)	1	0	1	1	1	1
	LSN	0	0	0	0	0	0
	LPI	0	0	0	0	0	0
	LPI_{ish}	--	--	--	--	--	--
	$D_{FS<1}$ (m)	--	--	--	--	--	--
Feb-11	S_{V1D} (mm)	3	0	1	1	3	1
	LSN	0	0	0	0	0	0
	LPI	0	0	0	0	0	0
	LPI_{ish}	--	--	--	--	--	--
	$D_{FS<1}$ (m)	--	--	--	--	--	--
Jun-11	S_{V1D} (mm)	1	0	1	1	1	1
	LSN	0	0	0	0	0	0
	LPI	0	0	0	0	0	0
	LPI_{ish}	--	--	--	--	--	--
	$D_{FS<1}$ (m)	--	--	--	--	--	--
Dec-11	S_{V1D} (mm)	1	0	1	1	1	1
	LSN	0	0	0	0	0	0
	LPI	0	0	0	0	0	0
	LPI_{ish}	--	--	--	--	--	--
	$D_{FS<1}$ (m)	--	--	--	--	--	--

Notes: $D_{FS<1}$ = Depth to the first liquefiable layer (FS_L<1) that is at least 200-mm thick, as determined by the Boulanger and Idriss (2016) liquefaction-triggering procedure (P_L=50%, C_{FC}=0.13, and $I_{c,cutoff}$ =2.6), and exported from *Cliq v.3.0.3.2*; undet. = the specified soil layer was not detected; Δ_{16976}, Δ_{5109}, Δ_{24500}, Δ_{24502}, Δ_{16978}, and Δ_{27495} indicate the amount of S_{V1D}, LSN, and LPI added to CPTs 16976, 5109, 24500, 24502, 1678, and 27495, respectively, due to the shallow penetration depths.

Note 7: Based on the borehole log (BH 16251, Figure 1), the groundwater table is at a depth of 1.6 m below the ground surface. The soil profile consists of (1) silty, ML, topsoil with organics to a depth of 0.4 m, (2) sandy silt, ML, the Yaldhurst member of the Springston formation, to a depth of 3 m, (3) gravelly fine to coarse sand, SW, the Yaldhurst member of the Springston formation, to a depth of 5.45 m, and (4) fine to medium sand, SP, of the Christchurch formation to a depth of 18.75 m (the end of the borehole).

Note 8: The ejecta-induced free-field settlement provided in Table 11 is an areal average settlement due to ejecta, which is based on the total settlement assessment area, A_T (provided in Table 9 and repeated in Table 14). However, the considered area was not always covered completely with ejecta; thus, it is important to provide the localized ejecta-induced settlement, too. The localized settlement due to ejecta is estimated using photographic evidence only as

$$S_{E,P\_localized} = \frac{V_E}{A_E}$$

where V_E is the total volume of ejecta within A_T and A_E is the total coverage area of ejecta within A_T. Please note that the areal ejecta-induced settlement provided in Table 14 as S_{E,P_areal} is the same as $S_{E,P}$ in Table 11, which was estimated as

$$S_{E,P\_areal} = S_{E,P} = \frac{V_E}{A_T}$$

where V_E is the total volume of ejecta within A_T and A_T is the total settlement assessment area.

Table 14a: Areal and localized ejecta-induced settlement estimates for Patch A (10-, 20-, and 50-m buffers) based on photographic evidence.

Earthquake Event	A_T (m^2)	A_E (m^2)	V_E (m^3)	S_{E,P_areal} (mm)	$S_{E,P\_localized}$ (mm)
Sep-10	49.8	0	0	0	0
Feb-11	49.8	43.1	2.6-4.3	70±15	80±20
Jun-11	49.8	20.6	0.8-1.2	20±5	50±10
Dec-11	49.8	0	0	0	0

Notes: S_{E,P_areal} = $S_{E,P}$ reported in Table 11 = areal ejecta-induced settlement; $S_{E,P\_localized}$ = localized ejecta-induced settlement; A_T = total settlement assessment area; V_E = total volume of ejecta within A_T; A_E = total area of ejecta within A_T; The estimates of both areal and localized ejecta-induced settlement are rounded to the nearest 5; Final plus/minus values are also rounded to the nearest 5.

Table 14b: Areal and localized ejecta-induced settlement estimates for Road (20-m buffer) based on photographic evidence.

Earthquake Event	A_T (m^2)	A_E (m^2)	V_E (m^3)	S_{E,P_areal} (mm)	$S_{E,P\_localized}$ (mm)
Sep-10	345	34.0	0.3-0.7	<5	15±5
Feb-11	349	348	11.3-14.2	35±5	35±5
Jun-11	327	113	2.0-4.0	10±5	25±10
Dec-11	349	0	0	0	0

Notes: S_{E,P_areal} = $S_{E,P}$ reported in Table 11 = areal ejecta-induced settlement; $S_{E,P\_localized}$ = localized ejecta-induced settlement; A_T = total settlement assessment area; V_E = total volume of ejecta within A_T; A_E = total area of ejecta within A_T; The estimates of both areal and localized ejecta-induced settlement are rounded to the nearest 5; Final plus/minus values are also rounded to the nearest 5.

Table 14c: Areal and localized ejecta-induced settlement estimates for Road (50-m buffer) based on photographic evidence.

Earthquake Event	A_T (m^2)	A_E (m^2)	V_E (m^3)	S_{E,P_areal} (mm)	$S_{E,P\_localized}$ (mm)
Sep-10	914	104	1.9-3.8	5±5	30±10
Feb-11	923	763	30.6-35.2	35±5	45±5
Jun-11	859	237	3.7-7.5	5±5	25±5
Dec-11	923	0	0	0	0

Notes: S_{E,P_areal} = $S_{E,P}$ reported in Table 11 = areal ejecta-induced settlement; $S_{E,P\_localized}$ = localized ejecta-induced settlement; A_T = total settlement assessment area; V_E = total volume of ejecta within A_T; A_E = total area of ejecta within A_T; The estimates of both areal and localized ejecta-induced settlement are rounded to the nearest 5; Final plus/minus values are also rounded to the nearest 5.

Summary 2:

- **The best estimate of the localized ejecta-induced free-field ground settlement at the Bideford Pl site for the SEP 2010, FEB 2011, JUN 2011, and DEC 2011 earthquake is 0 mm, 80±20 mm, 50±10 mm, and 0 mm, respectively. For the SEP 2010 earthquake, the localized ejecta-induced settlement for <5% of the site that had ejecta could not be estimated.**
- **The best estimate of the localized ejecta-induced free-field settlement of the road at the Bideford Pl site for the SEP 2010, FEB 2011, JUN 2011, and DEC 2011 earthquake is 15±5 mm, 35±5 mm, 25±10 mm, and 0 mm, respectively.**